

**Report 10300-12
September 1994**

**Earth Observing System (EOS)/
Advanced Microwave Sounding Unit-A (AMSU-A)
Monthly Report for August 1994**

**Contract No: NAS5-32314
CDRL 529: (Including CDRL 203, 204, and 503)**

Submitted to:

**National Aeronautics and Space Administration
Goddard Space Flight Center
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Section 1

INTRODUCTION

This is the twentieth monthly report for the Earth Observing System/Advanced Microwave Sounding Unit-A (EOS/AMSU-A), Contract NAS5-32314, and covers the period from 1 August 1994 through 31 August 1994. This period is the eighth month of the Implementation Phase which provides for the design, fabrication, assembly, and test of the first EOS/AMSU-A, the Protoflight Model. During this period the number one priority for the program continued to be the issuance of Requests for Quotations (RFQ) to suppliers and the procurement of the long-lead receiver components. Significant effort was also dedicated to preparation and conduct of internal design reviews and preparation for the PDR scheduled in September.

An overview of the program status, including key events, action items, and documentation submittals, is provided in Section 2 of this report. The Program Manager's "Priority Issues" are defined in Section 3. Sections 4 through 7 provide detailed progress reports for the Systems Engineering effort, each Subsystem, Performance Assurance, and Configuration/Data Management. Contractual matters are discussed in Section 8.

Section 2

GENERAL STATUS OF EOS/AMSU-A PROGRAM

This section presents an overview of the accomplishments and status of the EOS/AMSU-A program as of the end of August 1994 and includes four sections: (1) Key Accomplishments, (2) Overall Status, (3) Action Item Status, and (4) Documentation (CDRL) Status.

2.1 *Key Accomplishments*

Key accomplishments during this report period included:

Specifications and Statements of Work (SOW) For Long-Lead Components

Vendor conferences were held with:

Litton	-VCGDO
	-DRO
FEI	-TCXO (crystal oscillator)
PHONON	-SAW filter

Comments from these vendors are being evaluated for update of the specifications and statements of work prior to the issuance of the requests for quotations (RFQ).

A2 Reflector

The RFQ for the A2 reflector was issued this month to three vendors, Composite Optics (COI), Programmed Composites (PCI), and Texas Instruments.

Command and Data Handling

The Command and Data Handling (C&DH) breadboard testing has continued. Hardware check-out is complete and firmware coding/check-out is nearly completed.

Phase-Lock Oscillator (PLO)

Analysis of the PLO is continuing for electrical radiation hardness, thermal, mechanical/structural, and EMI/EMC. The VCGDO envelope drawing and updated specification have been signed-off and are ready for interim release for RFQ purposes.

Mechanical and Thermal

A1 and A2 module mechanical tolerance analyses have been completed.

Both A1 and A2 TRASYS and reduced SINDA thermal models have been completed.

Ground Support Equipment

It has been established that the NOAA/AMSU-A thermal calibration fixture can be modified for EOS, eliminating any need for a new fixture.

Internal Design Reviews

In an effort to maximize the EOS benefit from "Lessons Learned" on NOAA/AMSU-A and other programs, internal design reviews were started this month. The following reviews were completed:

- System Requirements/System Design
- DC-DC Converter
- Structural/Thermal
- Phase Locked Oscillator
- Ground Support Equipment
- Software
- Signal Processor
- Power Distribution
- Command and Data Handling
- Antenna Subsystem

The Receiver Subsystem will be reviewed the first week of September.

2..2 Overall Status

Critical path management continues to be utilized on EOS/AMSU-A to control program focus. The critical paths for the program are controlled by procurement of long-lead components. As reported last month, the following critical path components require purchase order placement in October 1994 through December 1994. Each has been annotated with the current procurement status.

1. VCGDO/Harmonic Mixer: Supplier conference complete, specification and SOW updated, RFQ issuance in September.
2. Crystal Oscillators (TCXO): Supplier conference complete, specification update in September, RFQ in October.
3. A2 Reflector: Specification and SOW updated, RFQ out, bids due in September.
4. DC/DC Converters: Delta proposals in, evaluation and selection in September.
5. SAW Filters: Supplier conference complete, specification update in September, RFQ in October.
6. DRO (Stable Oscillators): Supplier conference complete, specification update in September, RFQ in September.

A summary assessment of the schedule status of the key tasks is presented in Table I. As indicated, the overall status shows improved schedule performance. All of the behind-schedule tasks, including long-lead component specification preparation, will be completed in sufficient time to prevent any overall schedule effect.

Work has progressed on Group II, medium lead, system components during the month. The specifications for the A1 and A2 motors, resolver, and motor bearings have been completed and are in sign-off cycle. The mixer/IF amplifier specification has been reviewed by the vendor and comments are being evaluated.

Table I Key Tasks - Schedule Status Overview

Key Tasks	Schedule Status			Comments
	Behind	On	Ahead	
	-45%	-15%	+15%	+45%
Long-Lead Component Specifications and SOW		X		Key Receiver/PLO vendor conferences held.
Command and Data Handling		X		Breadboard hardware testing completed.
Software (Includes Firmware)		X		C&DH firmware being tested in breadboard.
DC/DC Converter		X		Delta proposals received.
Mechanical Design		X		Back on track for PDR.
Ground Support Equipment		X		VCGDO and TCXO supplier conference held.
Ground Support Equipment		X		Preliminary design on schedule for all GSE.

The EOS/AMSU-A Protoflight Master Schedule is shown in Figure 1. A copy of the design phase detailed schedules is presented in Appendix A.

2.3 Action Item Status

This section presents a summary of all action items that existed during this report period.

Copies of responses to all Aerojet action items submitted during this month are presented in Appendix B.

NASA action items from the 4, 5 May 1994 DCR are summarized in Table II.

Aerojet action items from the July 26, 27 Quarterly Review and July 27 Spacecraft Interface Meeting are presented in Table III. Twenty-six of thirty-five items have been completed.

NASA action items from the July 26, 27 meetings are summarized in Table IV.

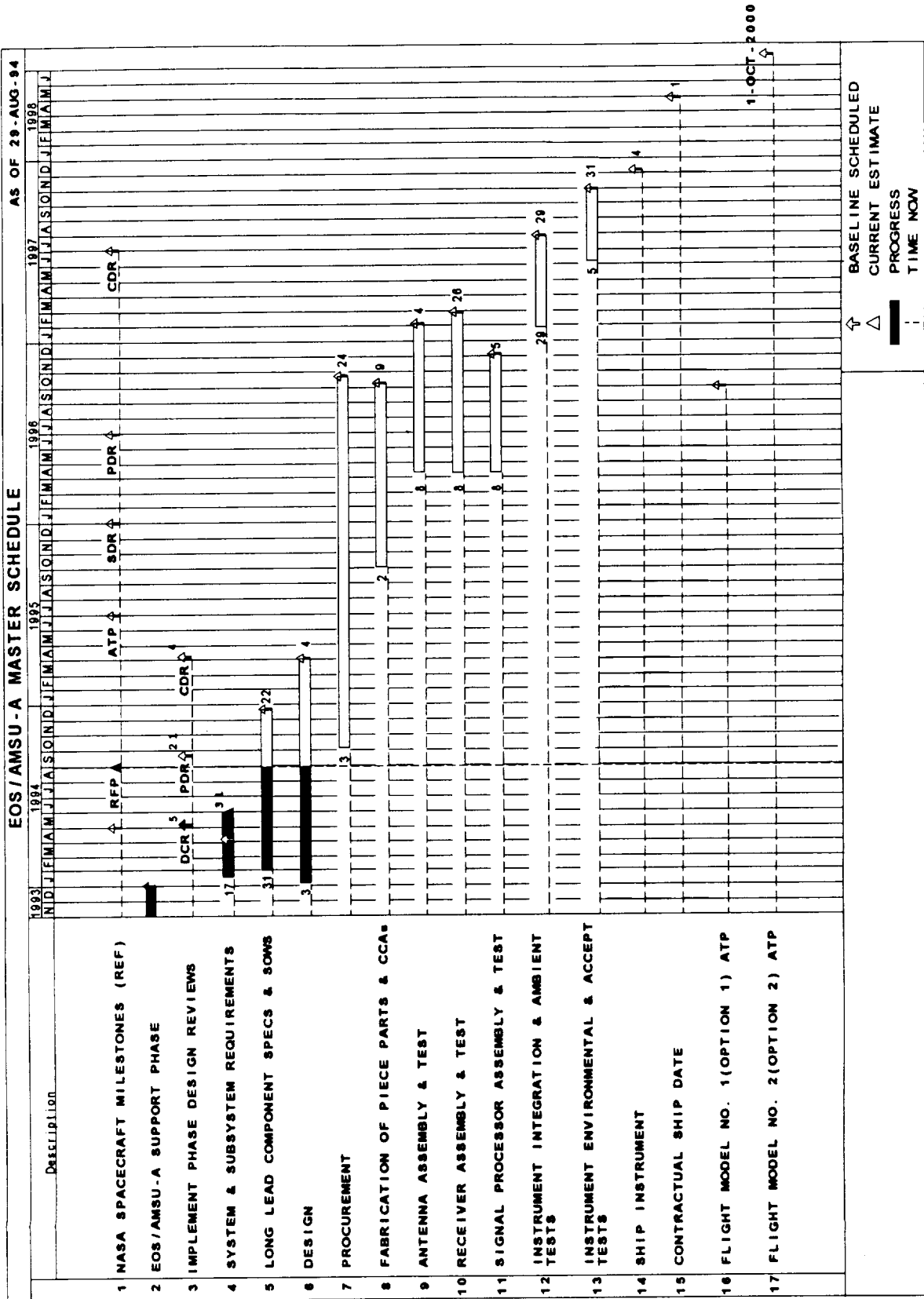


Figure 1 EOS/AMSU-A Master Schedule

**Table II Action Item Log - NASA
Design Concept Review of 4, 5 May '94**

Action Item No.	Description	Responsibility	Due Date	Disposition Date Ref. Doc.
5/5-20	1. Define Instrument offset Requirements. 2. Who implements? Instrument or Spacecraft?	NASA, EOS Project and JPL	6/15/94	June '94 In revised IDD (change 01)
5/5-21	Provide sample manufacturing Plan.	1. NASA will provide sample plan. 2. Aerojet is submitting Draft Plan at PDR, Final at CDR (submittals under CDRL 023 of existing contract). Will review sample plan and incorporate as required. Inputs are appreciated.	5/27/94	Faxed to D. Howell on 5/12/94
5/5-22	Review PAR Thermal Vacuum Testing Requirements and Aerojet Test Concepts.	NASA, EOS Project	6/15/94	7/17/94 NASA memo R. Shelly to M. Domen, copy Faxed to D. Howell, Aerojet
5/5-23	Provide Bandwidth for CEO 1/EO3 (Para. 10.11.1 of GIRD)	NASA, EOS Project	6/15/94	
5/5-24	Review STE Modification/Utilization Low Plan for EOS/NOAA Conflicts.	NASA, EOS Project	6/15/94	6/6/94 To be addressed as part of EOS/NOAA Contract merger.
5/5-25	Clarify GIRD Requirements Regarding "Science Data, Diagnostic Data, and Engineering Data". What Data goes in each category?	NASA, EOS Project	6/15/94	Will review Aerojet A1 5/5-10 response

Table IIIa Action Item Log - Aerojet
Quarterly Review and Spacecraft Interface Meeting of 26 & 27 July 1994

ACTION ITEM NO.	DESCRIPTION	RESPONSIBILITY	DUE DATE	DISPOSITION DATE, REF. DOC.
7/26-1	Spacecraft System Concept Review is planned for end of 1995. Aerojet should aim to start working ICD issues with spacecraft contractor starting two months after the scheduled award date of July '95. Final ICDs should be available at the SCR. Put this in ARTEMIS/PMS planning.	Don Howell/ Weldon Chapman	8/16/94	8/16/94 with Weekly Report
7/26-2	Schedule status "behind/ahead" (page 20). What is the metric for being within "on schedule". Define the metric.	Don Howell	9/1/94	8/3/94 in Weekly Report
7/26-3	System engineering schedule status (page 33). Add updates to ICD plan to post-PDR, post-CDR (if required) and the August-December '95 time frame for coordination with the spacecraft contractor (see A1 7/26-1) above).	Weldon Chapman	9/1/94	8/16/94 with Weekly Report
7/26-4	Provide data for COI bond line stress levels for launch loads.	Wayne Ely/ Steve Sherman	8/31/94	8/30/94 with Weekly Report
7/26-5	A2 reflector - Determine practicality of making engineering model of composite reflector (if selected) upgradable to a flight model.	Dennis Brest/ Steve Sherman	9/21/94	
7/26-6	Provide NASA with the date when we need inputs regarding the choice of the A2 reflector material (composites vs Beryllium).	Don Howell	8/2/94	8/1/94 Faxed to P. Pecori
7/26-7	Provide NASA a copy of the A2 reflector specification including specification drawing	Dennis Brest/ Don Howell	8/10/94	8/9/94 AI Response to Fed- X to T.O.
7/26-8	Look at efficacy of spending money on emissivity studies/discuss with project (calibration accuracy study, page 63)	Don Howell/ Dennis Brest	8/3/94	8/3/94 in Weekly Report
7/26-9	Hold conference call between Jim Parkinson and Bob Shelley/Mark Domen regarding flowdown of radiation specifications.	Don Howell/ Jim Parkinson	8/31/94 Bob S. on vaca 8/31	
7/26-10	Antenna motor bearings - define what is meant by "bake-out" on page 92.	Weldon Chapman/ Hal Cover	8/10/94	8/10/94 with Weekly Report
7/26-11	Provide a briefing on (1) How we track parts from purchase to "as-built configuration", (2) How we track GIDEP alerts. What are the computerized parts? How long does it take from identifying GIDEP part number to knowing if, and where, it is in our products?	Bob Mehlretter	9/21/94	
7/26-12	Keep Mark Domen informed of Aerojet's potential visits to sub-contractors so NASA may attend meetings as they desire.	Don Howell/ Al Nieto	Continual	
7/26-13	Present the project with a briefing of our DC/DC converter source selection.	Mark Pluck	9/21/94 (PDR)	
7/26-14	Request that when PAR is referenced use the "GSFC-420-05-01, Rev. A dated August 2, 1991". (To assure not referring to NOAA/AMSU-A PAR)	Bob Mehlretter/ PTLs	With issuance of revised PAIP & PDR presentation	

(Continued)

Table IIIa Action Item Log - Aerojet
Quarterly Review and Spacecraft Interface Meeting of 26 & 27 July 1994 (Cont.)

ACTION ITEM NO.	DESCRIPTION	RESPONSIBILITY	DUE DATE	DISPOSITION DATE, REF. DOC.
7/26-15	When stating a material, (coatings, epoxys, etc.) to be used, provide the name or part designation; e.g.; coating (Si O ₂).	Bob Mehlretter/ PTLs	With issuance of revised PAIP & PDR presentation	
7/26-16	Materials lists to be developed. Provide the data as requested by the GSFC-420-05-01 PAR in Figures 6-1C, 6-1D, 6-1E and 6-1F.	Bob Mehlretter	8/21/94 with CDRL 506 submittal	8/17/94 with CDRL 506
7/26-17	When discussing a thermal/vacuum test, state T/V. If we see only thermal listed, we assume NO vacuum.	Don Howell/ PTLs	Concur. Closed.	7/28/94 Concur
7/26-20	Modify CDRL status/tracking table to include a list of all submittals per each CDRL item and the category assigned. (Note: It was agreed Aerojet would provide a copy of their master CDRL schedules, includes all of above information.)	Don Howell	8/3/94	8/3/94 with Weekly Report
7/26-21	Provide list of schedule "Critical" parts and materials ASAP for expediting by GSFC. Submit NSPARs at least 30 days prior to procurement date.	Bob Mehlretter	8/10/94	8/10/94 Faxed to M. Domen, (with Weekly Report of 8/16/94)
7/26-22	Ensure that Parts and Materials Lists submitted to GSFC for approval include Aerojet's and all subcontractors' parts and materials lists.	Bob Mehlretter/ Hal Cover	8/21/94 with CDRL 506	8/17/94 with CDRL 506
7/26-23	Provide rationale for how Chapter 9, Contamination of the EOS Instrument PAR can be met while using a 100K clean room and stated visual inspections. Address why black light inspections and tape samples are not utilized.	Hal Cover	With submittal of CCP due at PDR	
7/26-24	Provide impact assessment of updated NSPARs submittal criteria	Bob Mehlretter/ Emil Lorenz	8/31/94	8/30/94 with Weekly Report

**Table IIIb Action Item Log - Aerojet
Spacecraft Interface Meeting of 27 July 1994**

ACTION ITEM NO.	DESCRIPTION	RESPONSIBILITY	DUE DATE	DISPOSITION DATE, REF. DOC.
7/27-1	What problem does going to 10V (from 8V) to the mixer/IF amp solve? Provide a list of SDARs. What is the supporting data that the problems are resolved?	Young Ma	8/31/94	8/31/94 Faxed to T.O.
7/27-2	Stop work on A1 weight reduction optimization design	Don Howell/ Wayne Ely	7/28/94	7/28/94 Program Directive No. 9
7/27-3	Be sure that bolts used on TIROS spacecraft are specified in the ICD.	Weldon Chapman	8/31/94 (Draft ICD)	8/23/94 with Weekly Report
7/27-4	Should the edge stiffening be implemented on the A2 to raise the natural frequency from 80Hz on the NOAA unit to 90 Hz on the EOS unit? What is trade between having to do additional analysis because we are less than 100 Hz and trying to get to 100 Hz? Include cost to do design change (including all paper and tests) and what is saved in production. Look at weight margin of N&N'.	Wayne Ely	8/31/94	8/30/94 with Weekly Report
7/27-5	What is relationship between linear (mils) shift in antenna motor shaft position and angle change (arc seconds).	Weldon Chapman	9/21/94	
7/27-6	Determine basis for 1553 RT validation plan.	Mark Pluck	8/11/94	8/10/94 with Weekly Report
7/27-7	Define current threshold on A/D convertor dropout.	Mark Pluck	8/31/94	8/10/94 with Weekly Report
7/27-8	See when we can get Gus Wessels, Mike Mitchell (and Don Howell) in the MRP training class.	Don Howell	8/15/94	8/10/94 FTDO Note to G. Wessels
7/27-9	Define what it takes to upgrade the CSTOL workstation to be capable of doing the complete instrument functions at the spacecraft contractors (not just listen only).	Bob Schwantje/ Doug McDonald	8/27/94	8/9/94 with Weekly Report
7/27-10	Review pyroshock and sine burst requirements and applicability to component and instrument.	Weldon Chapman/ Wayne Ely	8/27/94	8/16/94 with Weekly Report
7/27-11	Flowdown to suppliers' requirement for N ₂ atmosphere during thermal cycling tests.	Weldon Chapman	8/27/94	8/30/94 with Weekly Report
7/27-12	Develop and maintain a list of differences between N/N' and EOS; e.g., components, major active devices, etc. Pete Pecori would like the first cut in about two weeks.	Weldon Chapman	8/11/94	8/9/94 with Weekly Report

Table IV Action Item Log - NASA
Quarterly Review & Spacecraft Interface Meeting of 26 & 27 July 1994

<u>ACTION ITEM NO.</u>	<u>DESCRIPTION</u>	<u>RESPONSIBILI TY</u>	<u>DUE DATE</u>	<u>DISPOSITION DATE, REF. DOC.</u>
7/26-N1	Provide Apiezon-C vacuum/bake-out data from Goddard tests prior to PDR if possible.	Mark Domen/ Bob Shelley	8/21/94	Tests in process as of 9/12/94
7/26-N2	Advise Aerojet regarding the acceptability of specification changes provided in response to DCR action items.	Mark Domen		9/6/94 Telecon Domen/Howell
7/26-N3	PDR - Advise if the guidelines Aerojet is planning to use for PDR are acceptable.	Mark Domen	8/8/94 if not OK	8/8/94 Telecon: OK
7/27-N1	Provide a letter summarizing the recommendations and GIRD clarification resolved in the C&DH splinter meeting. Include clarification of how data is to be handled when request for data is not received from the spacecraft.	Mark Domen/ Pete O'Neill	8/21/94	9/6/94 Telecon Domen/Howell Ltr to follow
7/27-N2	Review the acceptability of 3°C/minute temperature change for component testing.	Bob Shelley	8/11/94	9/6/94 Telecon Domen/Howell
7/27-N3	Review the number of T/V and thermal cycles required.	Bob Shelley	8/11/94	9/6/94 Telecon Domen/Howell

2.4 Data Delivery

The Contract Data Requirement List (CDRL) items shown in Table V were delivered during this report period.

Table V EOS/AMSU-A August Documentation Submittals

CDRL	Description	Submitted to NASA
023	Fab/Assy Flow Plan	8/18/94
025	In-Flight Checkout Plan	8/17/94
108	FMEA	8/18/94
203	Configuration Management Status Report (Included in CDRL 529)	8/16/94
204	Performance Assurance Status Report (Included in CDRL 529)	8/16/94
303	Command List & Description	8/10/94
305	Engineering Telemetry Desc	8/12/94
306-2B	Firmware Requirements	8/1/94
308	Performance Verification Spec	8/3/94
309	Software Assurance Plan	8/18/94
403	* DPA Procedures	8/30/94
405	General Oper Command Proc	8/17/94
503	Weight/Power Budgets (Included in CDRL 529)	8/16/94
504	Limited Life Items List	8/18/94
506	Matl List, Lub List/Processes List	8/17/94
507	Critical Items List	8/18/94
521	Weekly Status Report	8/1, 8/9, 8/16, 8/23 & 8/30
523	Performance Measurement Status Report (Included in CDRL 534)	8/18/94
527	As-Designed Parts List	9/1/94
529	Reports of Work (Monthly Status Report)	8/16/94
534	Mo./Qrtly. Financial Mgmt. Rpt. (NASA Fm. 533M/533Q)	8/18/94
*Resubmittal based on NASA comments.		

Section 3

PRIORITY ISSUES

The Program Manager's current priority issues and concerns are presented in Table VII. The status and plan for each issue is included, together with general comments to assist in understanding the background or plans for each entry.

Table VI Program Priority Issues

Issues/Concerns	Status and Plan	Comments
PLO Configuration - Repackaging PLO to provide an integrated crystal oscillator/PLO package and reduce noise potential is being considered. Since crystal oscillator is a critical path item, issue must be resolved promptly.	Evaluation in process but PDR preparation is interfering. Will present plan at PDR.	Potential major improvement. Long term payoff potential very high.
Assure long-lead item purchase orders get placed on schedule - they control critical paths (Schedule slips cost approximately \$250K/month)	Critical paths have been updated. Work has been prioritized in accordance with critical paths.	See PLO item above. Other items moving on schedule for October through December purchase order placement.
Cost containment	Rates have stabilized.	Rates situation may be helped by SADARM success - could increase the direct labor base.
A-2 Module antenna material	Composites selected. Established competitive procurement strategy for composites. RFQs issued.	Potential suppliers preparing proposals. Proposal evaluation team established.
Command and Data Handling interface requirements. We are breadboarding early; must assure requirements are solidified and understood.	Discussion with NASA technical officer 18 August at Aerojet assures good requirements understanding. NASA will provide written confirmation of requirements.	Plan to complete breadboard tests prior to PDR.

Section 4

SYSTEMS ENGINEERING

Primary Systems Engineering activity for August included responses to action items, systems support in the preparation and review of component specifications and statements of work, establishment of guidelines and schedules for internal design reviews, and preparation and presentation of an internal system design review.

An initial draft of the Interface Control Document was completed. Team members have reviewed the document and submitted their comments. Final review of the Radiometric Math Model was completed and the document is being corrected and released for delivery to NASA.

Efforts continued to verify requirements allocation to subsystems and interfaces in support of critical path procurement activities and in preparation for internal design reviews.

Responses to Action Items 7/26-1, -3, -10, and -18 and 7/27-3 and -12 were completed and submitted to GSFC. Copies are provided in Appendix B.

Guidelines for Internal Design Reviews were prepared and provided to Product Team Leaders. Schedules for all internal reviews were then established, beginning with the Systems Internal Design Review.

An internal Systems Design Review was held on Wednesday, 24 August. A list of attendees and a summary of the review and action items are presented in Appendix C.

4.1 *Weight and Power Budgets (CDRL 503)*

Weight and power estimates, shown in Tables VII and VIII have changed since last month to reflect a more accurate estimate of the latest A1 mounting structure and the addition of the previously deleted upper card rack. This rack is not needed to hold circuit cards (which have been deleted) but was found necessary for thermal conduction and to a lesser degree, structural support.

Table VII EOS/AMSU-A WEIGHT BUDGETS AND ESTIMATES

Subassembly	AMSU-A1		AMSU-A2	
	Budgeted Weight (kg)	Estimated Weight (kg)	Budgeted Weight (kg)	Estimated Weight (kg)
Antenna	25	22.46	32	29.18
Receiver	16	13.90	4	2.00
Signal Processor	7	6.23	4	3.99
Power Distribution	2	1.59	2	1.59
Miscellaneous	7	4.56	7	3.75
Subtotals	57	48.74	49	40.51
Totals				
Estimated			89.25	
Budgeted			106	
Specification			110	

Table VIII EOS/AMSU-A POWER BUDGETS AND ESTIMATES

Subassembly	AMSU-A1		AMSU-A2	
	Budgeted Power (W)	Estimated Power (W)	Budgeted Power (W)	Estimated Power (W)
Antenna Scan Drive				
Noisy Bus	4	3.1	4	3.2
Quiet Bus	11	9.7	7	5.1
Receiver	36	34.3	5	4.9
Signal Processor	13	12.1	9	7.8
DC/DC Converter	19	18.2	7	5.8
Subtotals	83	77.4	32	26.8
UIID Allocation	88		37	
AMSU-A Totals				
Estimated	104.2			
Budgeted	115			
UIID Allocation	125			

Section 5

SUBSYSTEMS, ASSEMBLIES, AND EQUIPMENT

5.1 *Antenna Subsystem*

Antenna Subsystem Performance Confirmation

The S/N 104 antenna performance data has been tabulated and prepared in graphic form as a means of confirming the subsystem performance of the EOS/AMSU-A antenna design. Beam pointing accuracy data, Figures 2 and 3, show conformance with the EOS requirements for all beam positions and channels. The half power beamwidth data, shown in Figures 4 and 5, show that the beamwidths are within the specification requirement of 3.3 degrees \pm 10%. The measured channel-to-channel variance of the average beamwidth, Figure 6 data exceeds the NOAA/AMSU-A requirement of 0.33 degree by 0.17 degree. A plan for mitigating this problem on future instruments is being formulated and will be presented at PDR. Beam efficiency, calculated from measured data, meets or exceeds requirements (\geq 95 percent) for all beam positions and channels.

Cold calibration antenna patterns were measured for the NOAA/AMSU-A S/N 104 instrument and calculations of the percent energy from the Earth during cold calibration were made for both the NOAA orbit and the EOS orbit. The calculations for EOS show that the antenna meets the derived requirement of \leq 0.70 percent. These data are presented in Figure 7 with a sample antenna pattern showing the sidelobe region which intercepts the Earth.

The motor performance for both the A1 and the A2 motors is shown in Figures 8 through 11 from measured S/N 103 motor data. In all cases the motors pass all specification requirements.

A2 Reflector Procurement Status

Two bidders, Composite Optics Incorporated (COI) and Programmed Composites Incorporated (PCI) have indicated they will respond to the request for proposal from Aerojet. The third vendor, Texas Instruments, has informed us of their "no-bid" decision due to the fixed price development required. Meetings have been set up with both remaining bidders to review the specification and SOW and answer any questions regarding interpretation of the requirements. The meetings will be held on Thursday, September 8 and Monday, September 12.

Motor and Bearing Procurement Status

The antenna product team will visit Vernitron Corporation in September to inspect their facility's readiness to manufacture and assemble space qualified parts and review the hardware specifications.

The bearing drawings have been reviewed for EOS and will be sent to Barden for quote. It is planned to instruct the bearing vendor to drop-ship their parts directly to the cleaning/lubrication vendor eliminating the need for an extra inspection and handling at Aerojet.

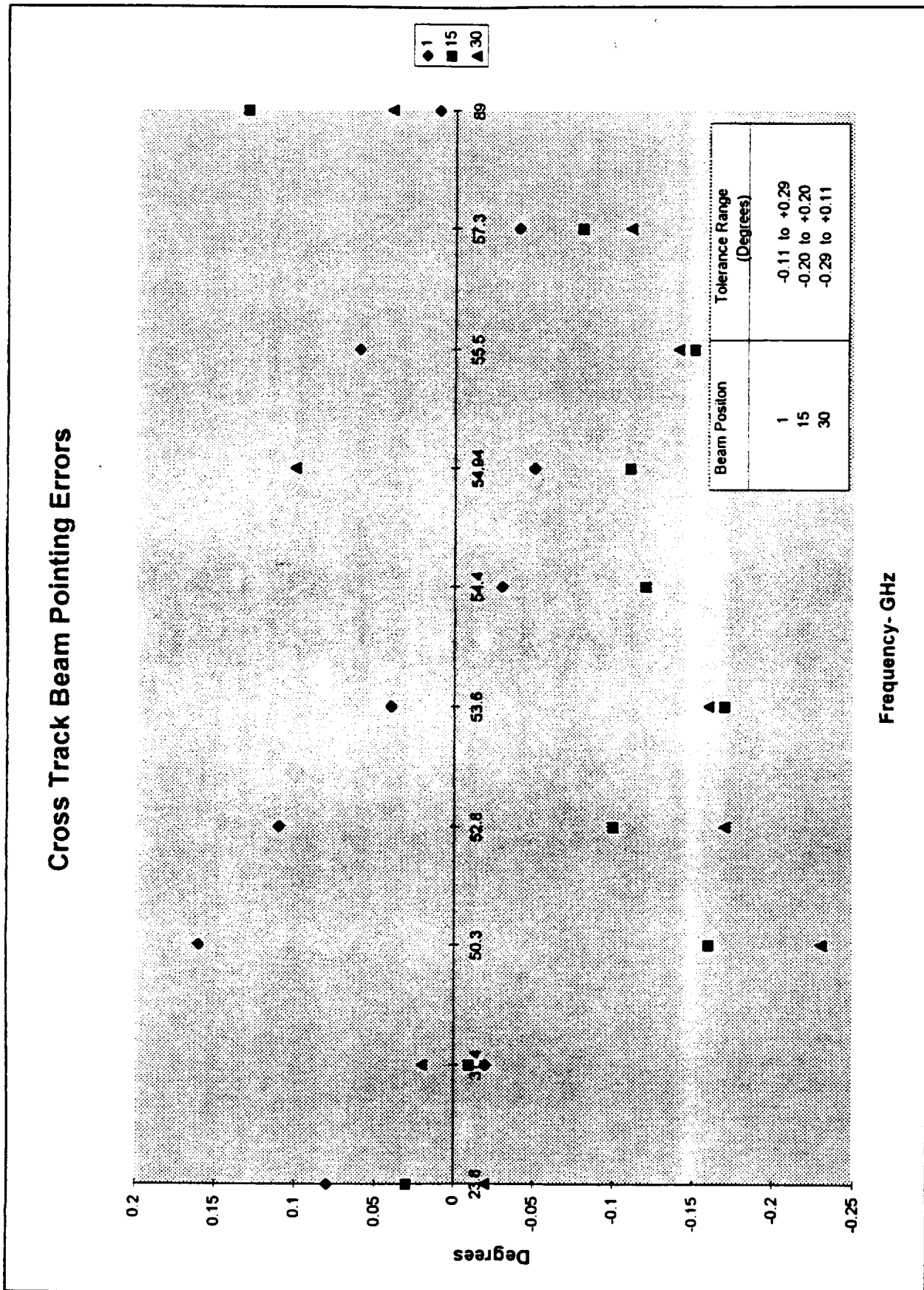


Figure 2 Beam Pointing Accuracy - Cross Track

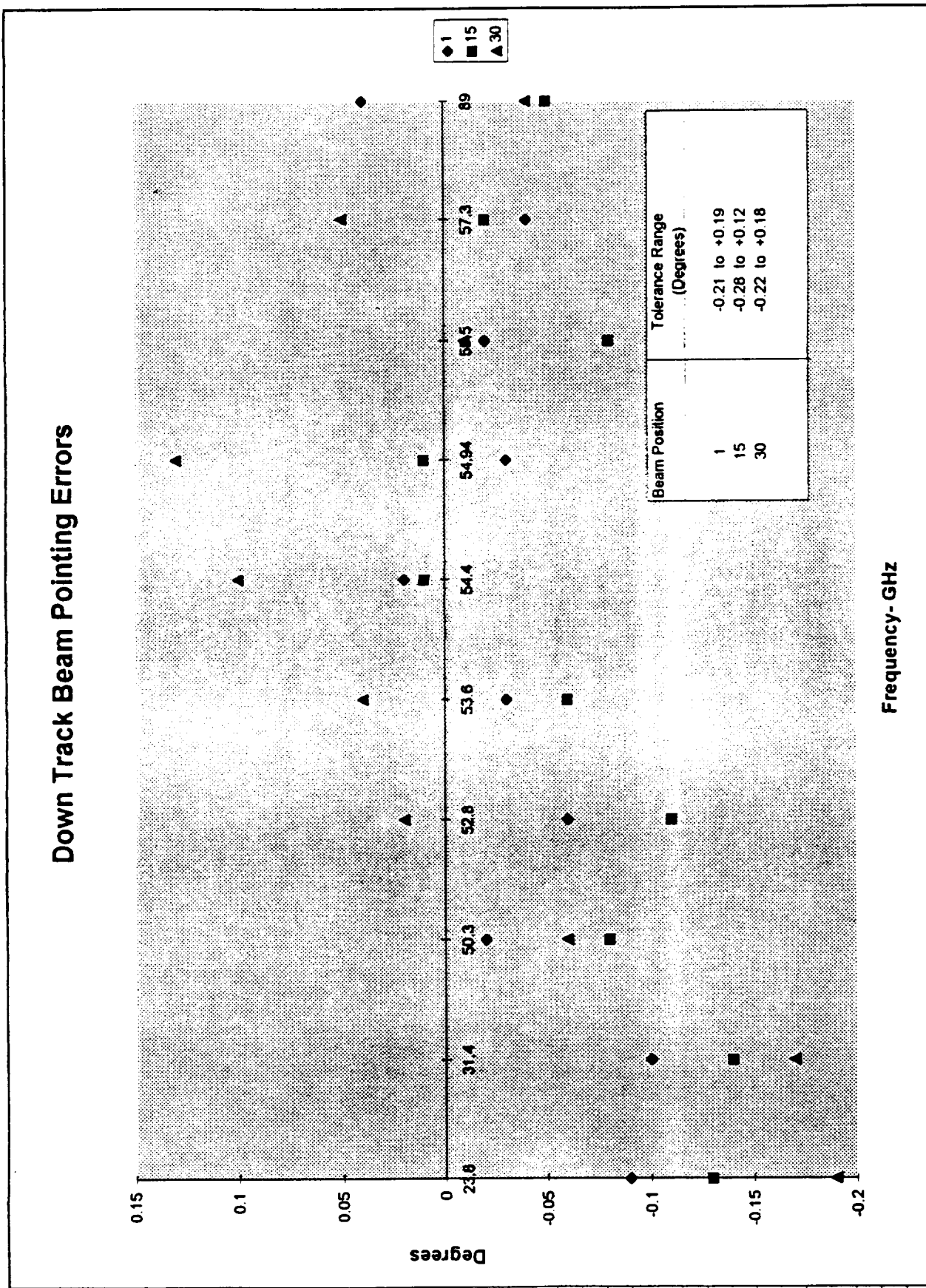


Figure 3 Beam Pointing Accuracy Down Track

Cross Track Beamwidths

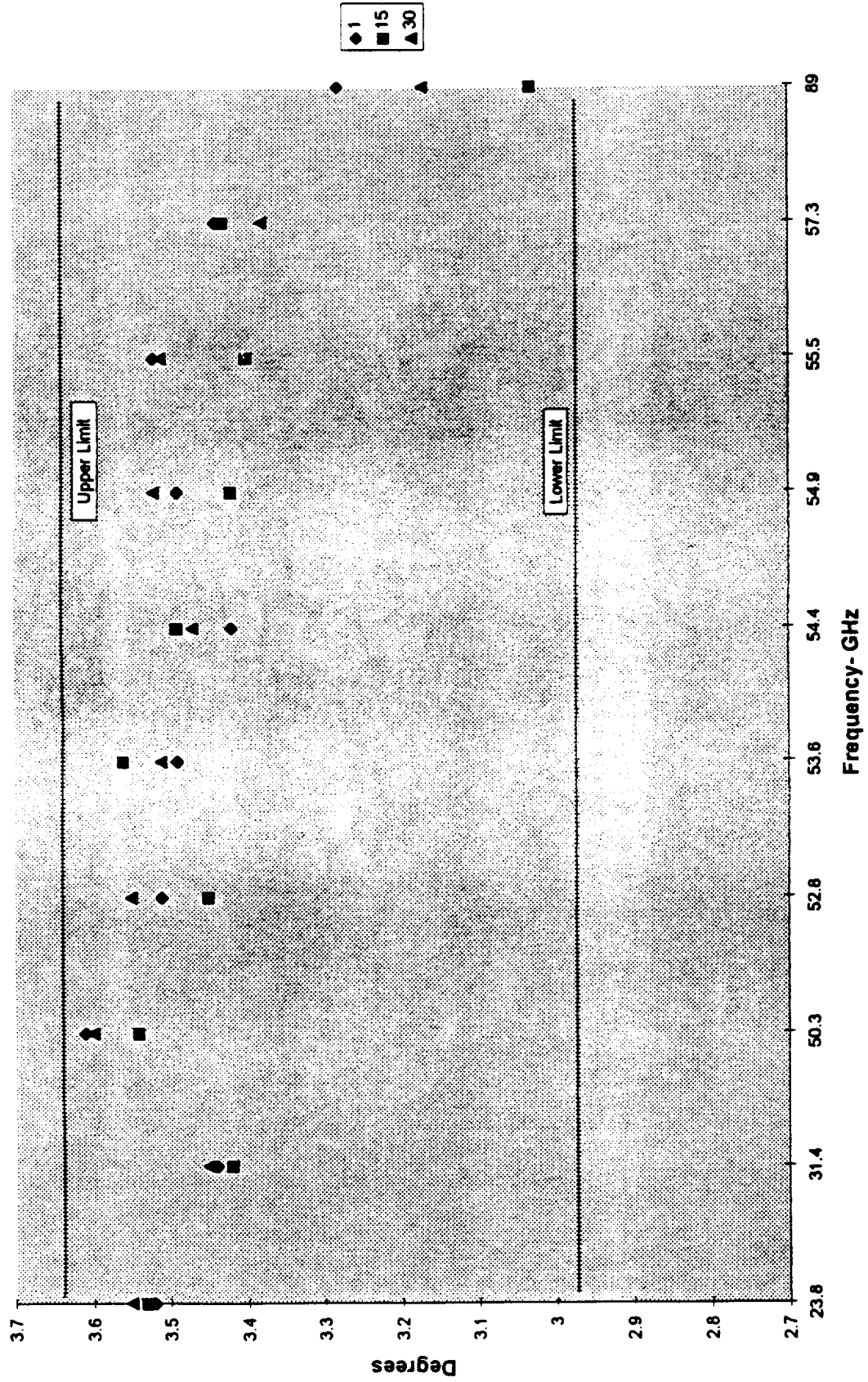


Figure 4 Beamwidth - Cross Track

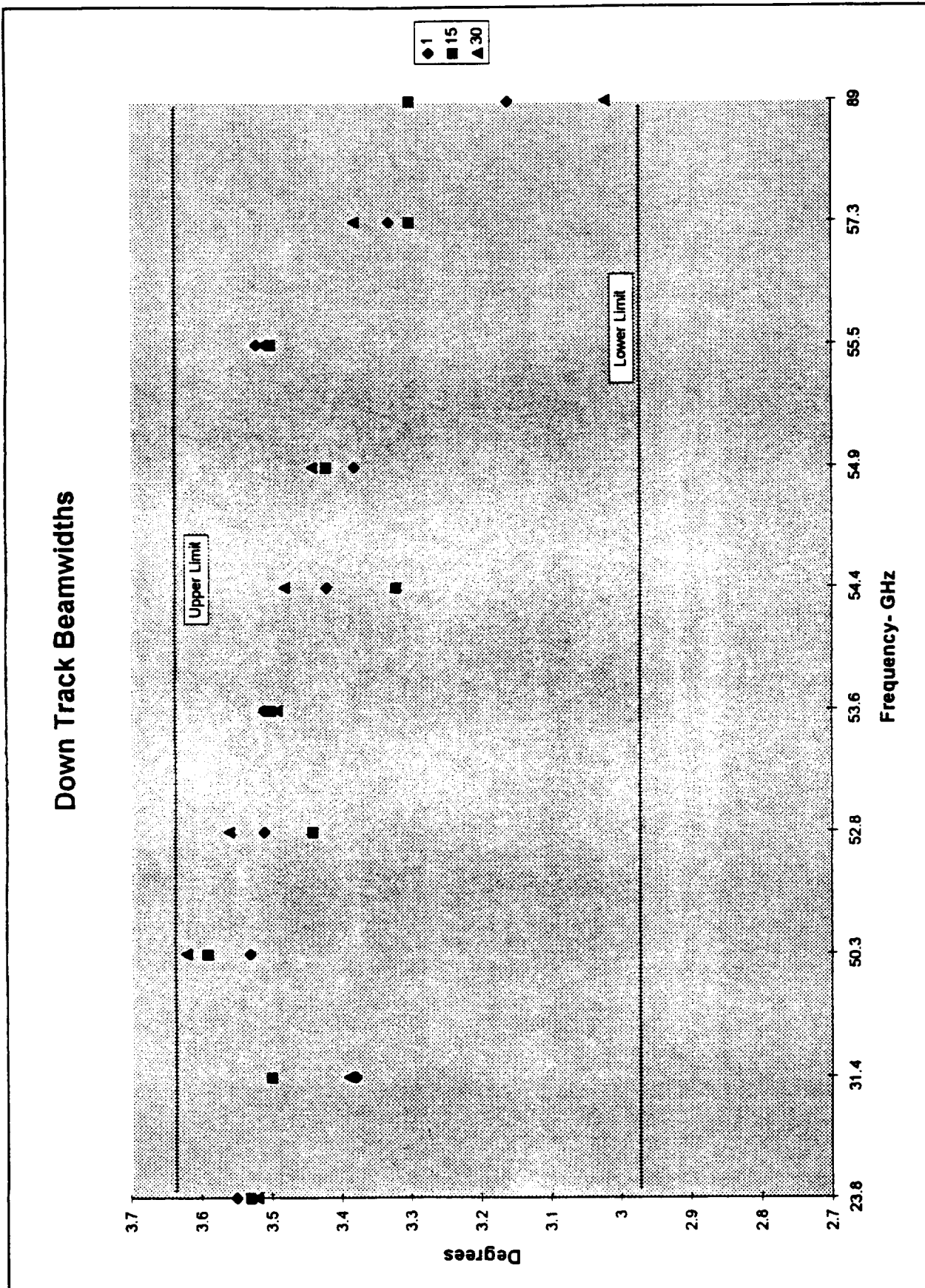


Figure 5 Beamwidth - Down Track

Channel-to-Channel Variance- Average Beamwidth

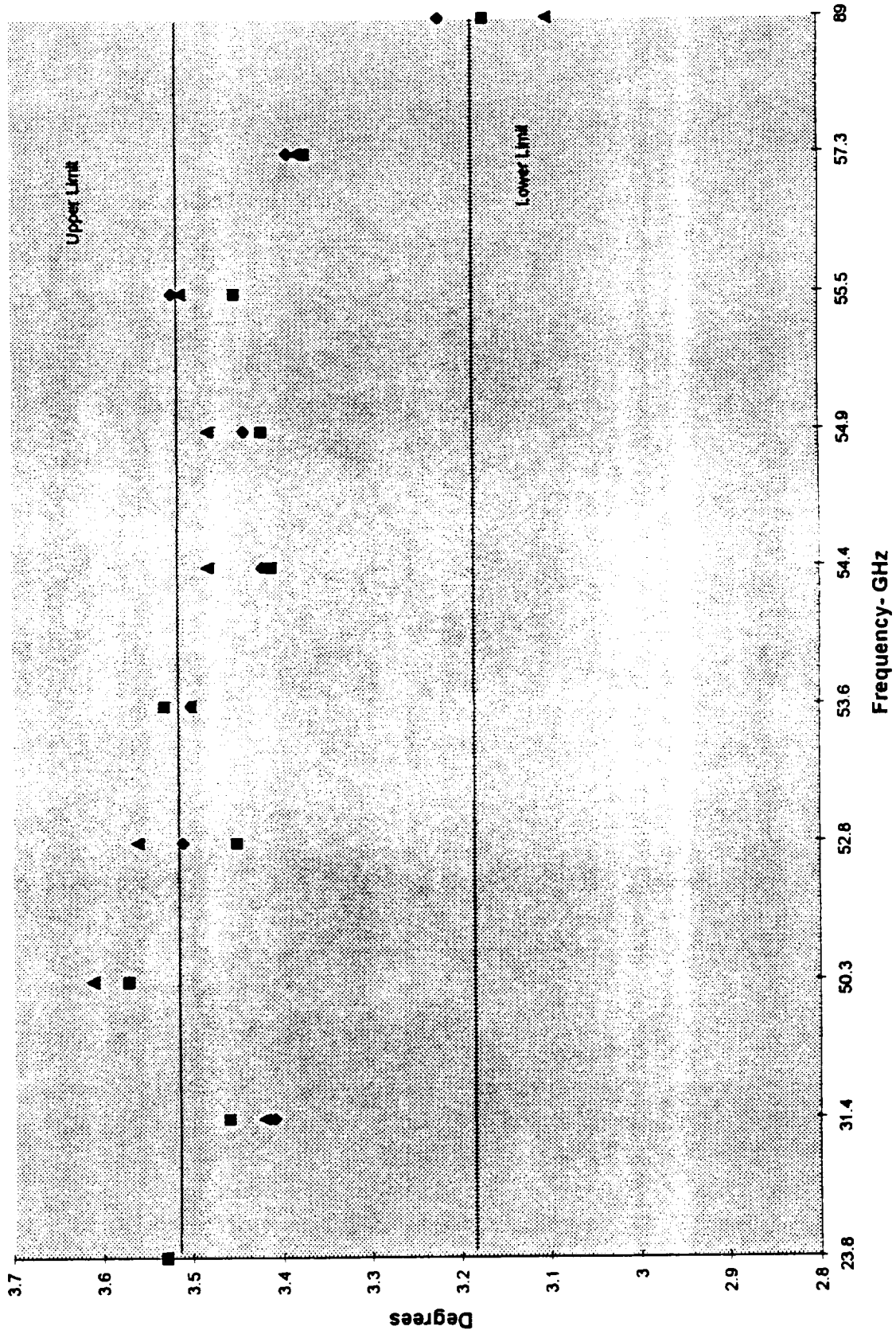
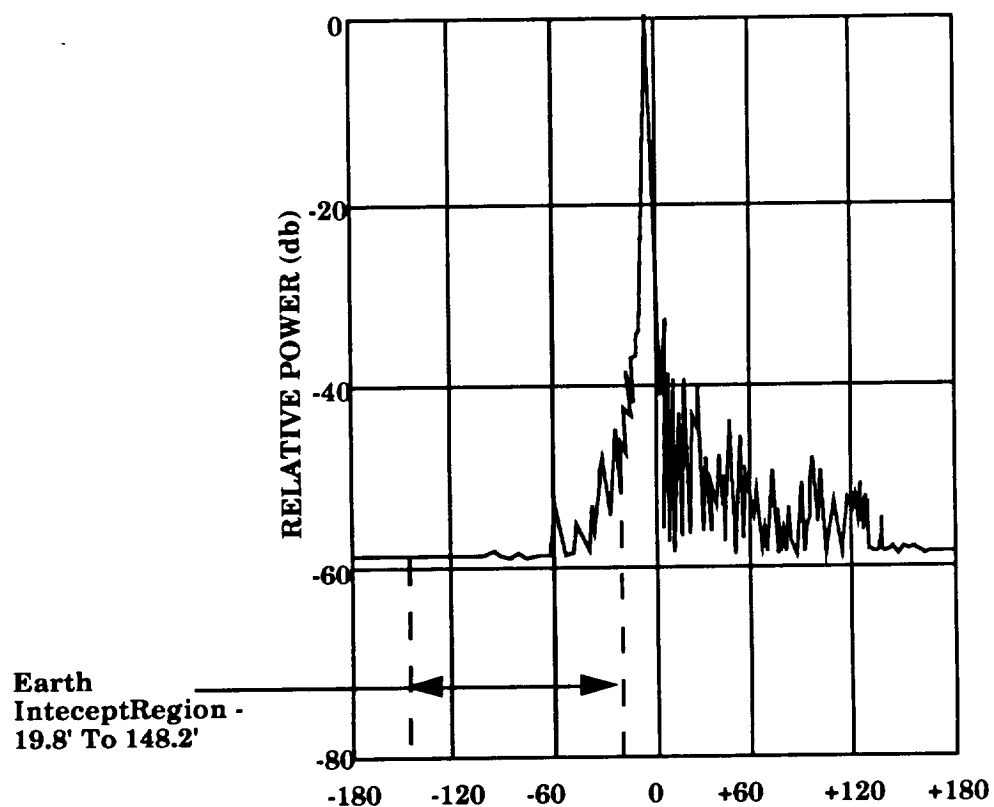


Figure 6 - Beamwidth Variance

Cold Calibration Data (S/N 104)

Frequency (GHz)	Percent Energy Required	Seeing Earth Measured
23.8	≤ 0.70	0.63
31.4	≤ 0.70	0.30
50.3	≤ 0.70	0.57
52.8	≤ 0.70	0.59
53.6	≤ 0.70	0.52
54.4	≤ 0.70	0.63
54.9	≤ 0.70	0.53
55.5	≤ 0.70	0.51
57.3	≤ 0.70	0.60
89.0	≤ 0.70	0.42

**Figure 7 Cold Calibration Data**

**AMSU-A1 Performance Verification Matrix
S/N 103**

Parameter Requirement (specification)	Measured Or Analysis Data	Verification Method				Level				Status
		T E S T	A N A L Y S I S	I N S P E C T I O N	D E S I G N	I N S T R U M E N T	I N T E G R A T I O N	A S S E M B L Y	S U B A S S E M B L Y	
S-480-13 Para. 3.6.3 Antenna Scan Performance										
8 second scan period	verified	X				X				comply
Scan synchronization	verified	X			X	X		X		comply
Maximum antenna jitter +10% -5% for 10 msec ± 5% for balance	A1-1 = 7.0% A=1-2 = 7.0%	X				X				comply
Sample Period Coincident	coincident 200ms sample period for each channel	X				X				comply
Equal Integration For Scene Calibration Samples	165 ms for A1	X				X				comply

Figure 8 A1 Motor Performance (S/N 103)

AMSU-A1 Performance Verification Matrix
S/N 103

S-480-13 Para. 4.5 Mechanical Requirements

Parameter Requirement (specification)	Measured Or Analysis Data	Verification Method				Level				Status
		T E S T	A N A L Y S I S	I N S P E C T I O N	D E S I G N	I N S T R U M E N T	I N T E G R I T Y	A S S E M B L Y	S U B A S E M B L Y	
S-480-13 Para. 4.5.3 Scan Mechanisms										
Torque Margin: >3 Times Worst Case Frictional Torque			X						X	comply
Motor Stall Vulnerability No Damage for 30 Min. Under Locked Condition	verified		X					X		comply
Motor Type Brushless	verified			X	X			X		comply
Encoding	verified	X		X		X		X		comply
Stability Margin A1-1: Gain =9.0dB/Phase = 25 Deg	10,00dB/68.8 Deg.	X					X			comply
Stability Margin A1-2: Gain =9.0dB/Phase = 25 Deg	9.24dB/67.6 Deg	X					X			comply
Caging/Deployment Not Desired	verified			X	X	X			X	comply
No Pyrotechnic	verified					X	X			comply

Figure 9 A1 Motor Performance (Continued)

**AMSU-A2 Performance Verification Matrix
S/N 103**

Parameter Requirement (specification)	Measured Or Analysis Data	Verifica- tion Method				Level				Status
		T E S T	A N A L Y S I S	I N S P E C T I O N	D E S I G N	I N S T R U M E N T	I N T E G R A T I O N	A S S E M B L Y	S U B A S S E M B L Y	
S-480-13 Para. 3.6.3 Antenna Scan Performance										
8 second scan period	verified*	X				X				comply
Scan synchronization	verified*	X			X	X		X		comply
Maximum antenna jitter +10% -5% for 20 msec ± 5% for balance	9%	X				X				comply
Sample Period Coincident	coincident 200ms sample period for each channel	X				X				comply
Equal Integration For Scene Calibration Samples	158 ms	X				X				comply

* Verified per AE-26156/4

Figure 10 A2 Motor Performance (S/N 103)

**AMSU-A Performance Verification Matrix
A-2 S/N 103**

S-480-13 Para. 4.5 Mechanical Requirements

Parameter Requirement (specification)	Measured Or Analysis Data	Verification Method								Level	Status
		T E S T	A N A L Y S I S	I N S P E C T I O N	D E S I G N	I N S T R U M E N T	I N T E G R A T I O N	A S S E M B L Y	S U B A S S E M B L Y		
S-480-13 Para. 4.5.3 Scan Mechanisms											
Torque Margin: >3 Times Worst Case Frictional Torque	>10 times	X	X						X		comply
Motor Stall Vulnerability No Damage for 30 Min. Under Locked Condition	verified		X					X			comply
Motor Type Brushless	verified*			X	X			X			comply
Encoding	verified**	X		X		X		X			comply
Stability Margin A2: Gain =12 dB/Phase = 25 Deg	16.9 dB/81.5 Deg.	X					X				comply
Caging/Deployment Not Desired	verified			X	X	X			X		comply
No Pyrotechnic	verified					X	X				comply

* Verified per AE-26052

** Verified per AE-26156/4

Figure 11 A2 Motor Performance (Continued)

5.2 Receiver Subsystem

5.2.1 General

Supplier conferences were held for all Group I long-lead receiver components during this reporting period. Litton visited Aerojet on August 2, 1994, to review the interim-release documents for the DRO and VCGDO/harmonic mixers and Aerojet visited Phonon at Simsbury, CT, for the SAW filters, and FEI at Michel Field, NY, for the crystal oscillators on August 16 and 17, 1994, respectively. Several issues and concerns were discussed in the meetings. Per our request, Phonon has conducted a test for the insertion loss variation with temperature on the NOAA/AMSU-A spare SAW filter units to evaluate the extended temperature range required for the EOS/AMSU-A SAW. The measured insertion loss variation of the lower passband was much higher than that of the higher passband (0.84 db vs 0.30 dB for -1 unit and 0.31 dB vs 0.03 dB for -4 unit over the temperature range from 0°C to +40°C). Phonon requested that the specification for insertion loss variation be applied to the average value of the two passbands instead of each passband.

Lessons-learned meetings were held with the NOAA/AMSU-A project and hardware integration team as part of the specifications review for the long-lead receiver components. The NOAA team reported a recent observation that increased system NE Δ T was seen when a DRO was operated in parallel with a GDO from a common power supply. The cause of the increase is not clear at this time and is being investigated.

The Product Specification and SOW of the IF amplifiers have been updated and are in review cycle.

Investigation of the DRO noise impact on the system temperature sensitivity has been completed. The DRO shows similar output spectrum characteristics as the GDO (See Figures 12 and 13). The noise figure and noise variance of the mixer measured with the DRO as the LO were comparable of slightly better than those measured with the GDO. This indicates that the NE Δ T will not degrade when DROs replace the GDOs that are used in NOAA/AMSU-A instruments for EOS.

Preparation began for the Internal Design Review (IDR) for the receiver subsystem. The IDR is scheduled on September 7, 1994 and will also serve as a dry run for the PDR. Response to Action Item 7/27-1 was completed and submitted.

5.2.2 Phased-Locked Oscillator (PLO)

The mechanical drawing package was reviewed during this month, and the resulting redlines are being incorporated into the drawings. The VCGDO/Harmonic Mixer envelope drawing was accelerated through the cycle and has been released to support the procurement of the VCGDO/Harmonic Mixer from Litton Solid State. The PLO electrical drawings are still in the check queue.

The VCGDO/Harmonic Mixer specification was reviewed with Litton Solid State personnel and several useful comments resulted in improvements in the specification. The VCGDO/Harmonic Mixer specification, statement-of-work, and envelope drawing have been signed-off and released and will be given to Litton for formal quotation in September.

The thermal, mechanical, and EMI analyses were completed and are ready for presentation at PDR. The reliability analysis is underway and will be completed by PDR.

Aerojet personnel visited Frequency Electronic Inc. (FEI) to solicit comments and concerns regarding the Crystal Oscillator specification. These inputs are being reviewed and evaluated and may result in modifications to the specification.

A PLO Internal Design Review (IDR) was held during this month. The IDR had two agendas. The first was to expose the PLO design to review from qualified technical areas outside the EOS/AMSU-A program. The second was to gather information and data for the PDR. The IDR resulted in many worthwhile comments that are currently being reviewed and considered. Of particular importance is a suggested repackagng concept which integrates the crystal oscillator within the PLO package, thereby reducing the risk of spurious noise sources affecting systems level performance.

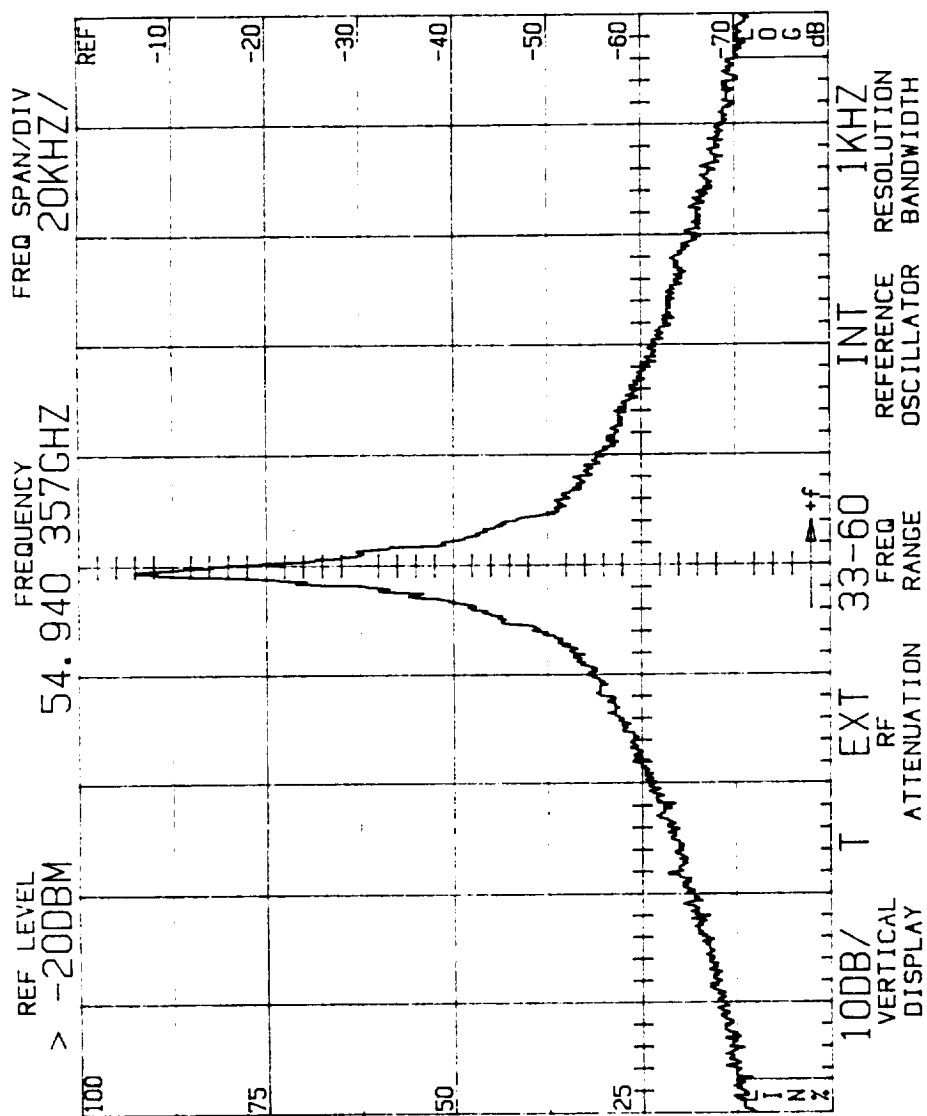


Figure 12 DRO Output

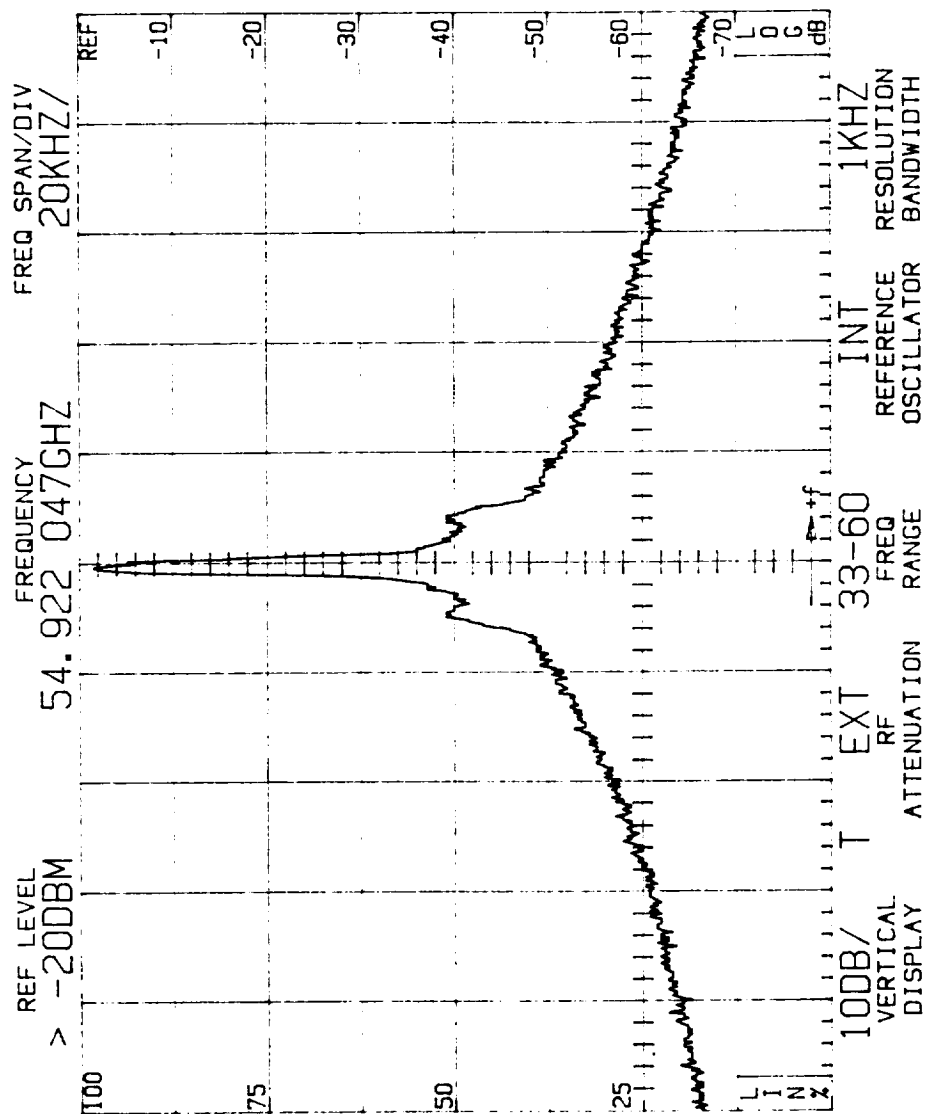


Figure 13 GDO Output

5.3 *Signal Processing Assemblies*

All hardware functions of the MIL-STD-1553 Interface breadboard have been checked out and are operational. The only correction to the design was a change in one wire to avoid an address contention. Interface firmware design was completed and the firmware loaded into the breadboard setup. Integration of the firmware with the hardware is progressing well with no major problems discovered to date. To work around a potential bottleneck in bringing on line the PC/MIL-STD-1553 bus analyzer, a rented standalone bus analyzer has been obtained. Checkout activity towards the end of the month slowed because of IDR and PDR preparation work.

Fabrication of the Signal Processor Test Set is 90 percent complete. This unit will be used as a universal test set for CCA and complete Signal Processor Assemblies.

During the month of August, the Signal Processor Team also supplied extensive assistance in the generation of the following CDRL items:

- CDRL 303 - Command List Description Update
- CDRL 305 - Engineering Telemetry Description Update
- CDRL 405 - General Operational Command Procedure

5.4 *Power Distribution*

An internal Design Review for the DC/DC Converter was held and it was decided to review the receiver power portion after a concern was raised regarding the use of a common power supply for the Local Oscillators. The need for, and impact of, reverting to independent local oscillator supplies is being examined. In the NOAA/AMSU-A instrument these supplies are required to be independently adjustable in order to tune the Gunn Diode Local Oscillators. EOS/AMSU-A uses Dielectric Resonance Oscillators (DROs) which are largely unaffected by supply voltage changes. The EOS/AMSU-A DROs will also include internal voltage regulators and a current foldback feature.

Work on the interconnection system made good progress with the first Engineering cable drawings and wire lists completed. A highly experienced packaging engineer has been brought on board to assist with connector selection and also to handle the interface between the mechanical and electrical aspects of the instrument internal wiring.

5.5 *Mechanical/Thermal Design Analysis*

The Mechanical/Thermal Integrated Product Team (IPT) members reviewed the Action Items from the EOS Quarterly Review held on 27 July. The responses for four Action Items- A1 7/26-4, A1 7/27-4, A1 7/27-5, and A1 7/27-10, were prepared by IPT. The team recommend that the component sine burst and pyroshock tests be eliminated. This Action Item was completed early to minimize the impact to already released and yet-to-be released component specifications.

The Mechanical/Thermal IPT reviewed work on the A1 Thermal Calibration Fixture and its interaction with the A1 module. The work progressed to the point where it was proven that the NOAA Thermal Calibration Fixture could be modified for EOS use instead of designing and building a brand new fixture.

Later in the month the Mechanical/Thermal IPT meetings concentrated on planning for the Internal Design Review that was held on 30 August. The review was in two sequential parts, Thermal and Mechanical/Structural. Most of the comments from the review team had to do with clarification and amplification of the presentations so that the NOAA/AMSU-A heritage was clear.

Additional technical material will be added to help non-EOS PDR personnel understand the evolution and status of the design.

Three action items were recorded from the review. One requested verification of the highest temperature required in the Motor Specifications versus the temperatures presented. Another requested that Aerojet reduce the potential technical risk from the pyroshock environment by determining the shock-sensitive components and applying an attenuated pyroshock spectrum to those components. The final action was to review the NOAA A2 reflector clamp and determine if a better clamp could be used.

Mechanical tolerance analysis of the A1 module and of the A2 module were completed during the month. The output was used as part of the worst case beam pointing error analysis to be included in the deliverable Worst Case Analysis.

The A2 stress analysis was completed and the Report technical input was submitted to the Technical Publishing group. Work was started on the A2 NASTRAN model description.

Both A1 and A2 TRASYS and reduced SINDA thermal math models were completed. The input for the deliverable Thermal Math Model Report was completed. A single report covered both the A1 and A2 models. Both models were subjected to check cases as required by the GIRD. The 32 degree sun angle (hot case) was run for both models. Conversion cards to change the models from English units to SI units as required by the GIRD were generated.

The PLO structural math model was completed and checked out during the week. Stress analysis using this model was used to determine design margins of PLO.

The mechanical team inputs to the deliverable ICD were integrated into the first draft of the document.

5.6 Ground Support Equipment

An Internal Design review for the EOS Instrument Ground Support Equipment (IGSE) was held on August 30. The review encompassed a description of the overall requirements for IGSE contained in various program documents followed by detailed requirements and design approaches for:

1. Handling fixtures
2. Drill templates
3. Manufacturing and protective equipment
4. Shipping containers
5. Calibration test equipment
6. Test fixtures
7. Special test equipment
8. Spacecraft interface workstation

The level of detail in the presentation was aimed at providing an understanding of program requirements for the various elements of the IGSE and a description of the general method whereby the requirements will be met using sketches, simplified block diagrams, and 3-D representations. The information presented was believed to be sufficient to allow the next stage to proceed whereby sheet metal designs, fixture details, wire lists, and cable design drawings could be prepared.

5.7 *Software*

During this reporting month, the coding of the command and data handling firmware was completed and has since been loaded into our microprocessor development system for checkout. A MIL-STD-1553 bus analyzer has been obtained and will be used for firmware testing.

CDRL 033a and 033b have been updated to incorporate NASA comments and will be submitted in early September.

The preliminary test procedure documents, CDRL 415a and 415b, have been drafted and are in review. They will also be submitted in early September.

PERFORMANCE ASSURANCE (CDRL 204)**6.1 *Quality Assurance***

Priority Quality Assurance activity for this month continued to be the review and approval of critical component specifications and statements of work.

6.2 *Design Assurance*

The following documents were completed during the month:

CDRL 506	Materials, Processes, and Lubricants List
CDRL 108	FMEA
CDRL 507	Critical Items List
CDRL 504	Limited Life Items

Section 7

DOCUMENT AND CONFIGURATION/DATA MANAGEMENT

7.1 Configuration Management

During this reporting period, there were no Configuration Management activities to report.

7.2 Document/Data Management

During this reporting period, Aerojet made sixteen Contract Documentation Requirement Listings (CDRL) submittals as shown in Table IX.

Table IX EOS/AMSU-A August Documentation Submittals

CDRL	Description	Submitted to NASA
023	Fab/Assy Flow Plan	8/18/94
025	In-Flight Checkout Plan	8/17/94
108	FMEA	8/18/94
203	Configuration Management Status Report (Included in CDRL 529)	8/16/94
204	Performance Assurance Status Report (Included in CDRL 529)	8/16/94
303	Command List & Description	8/10/94
305	Engineering Telemetry Desc	8/12/94
306-2B	Firmware Requirements	8/1/94
308	Performance Verification Spec	8/3/94
309	Software Assurance Plan	8/18/94
403	* DPA Procedures	8/30/94
405	General Oper Command Proc	8/17/94
503	Weight/Power Budgets (Included in CDRL 529)	8/16/94
504	Limited Life Items List	8/18/94
506	Matl List, Lub List/Processes List	8/17/94
507	Critical Items List	8/18/94
521	Weekly Status Report	8/1, 8/9, 8/16, 8/23 & 8/30
523	Performance Measurement Status Report (Included in CDRL 534)	8/18/94
527	As-Designed Parts List	9/1/94
529	Reports of Work (Monthly Status Report)	8/16/94
534	Mo./Qrtly. Financial Mgmt. Rpt. (NASA Fm. 533M/533Q)	8/18/94
*Resubmittal based on NASA comments.		

7.3 Scheduled Submittals

In accordance with the EOS/AMSU-A Master CDRL Schedule, the CDRL items listed in Table X will be submitted to NASA during the months of September and October 1994.

Table X EOS/AMSU-A September/October Documentation Planned Submittals

CDRL	Description	Due to NASA	Submitted to NASA
	September 1994:		
007	Contamination Control Plan	9/21/94	*
008	Software Management Plan	9/21/94	
016	PDR Data Package	9/21/94	
017	Software PDR Data Package	9/20/94	
018	Calibration Management Plan	9/21/94	
033	Software Test Plans:		
	Software Test Plan (Firmware)	9/21/94	9/1/94
	Software Test Plan (GSE)	9/21/94	9/1/94
035	Spares Program Plan	9/21/94	
101	Radiometric Math Model	9/21/94	
102	Structural Math Models:		
	Structural Math Model A1	9/21/94	
	Structural Math Model A2	9/21/94	
103	Thermal Math Models:		
	Thermal Math Model A1	9/21/94	
	Thermal Math Model A2	9/21/94	
106	Hazard Analyses	9/21/94	
113	Stress Analyses Reports:		
	Stress Analyses Report A1	9/21/94	
	Stress Analyses Report A2	9/21/94	
203	Configuration Management Status Report (Included in CDRL 529)	9/15/94	
204	Performance Assurance Status Report (Included in CDRL 529)	9/15/94	
302	Instrument Functional Logic Dia	9/21/94	9/1/94
306-2A	Spec Test Equip. SW Req.	9/21/94	
306-3A	S/W Architecture Design Doc	9/21/94	
402	S/W Standards/Procedures:		
	S/W Dev Process Manual	9/20/94	
	S/W Dev Standards Manual	9/20/94	
	S/W Dev Procedures Manual	9/20/94	
415	S/W Test Procedures:		
	S/W Test Procedure (Firmware)	9/21/94	
	S/W Test Procedure (GSE)	9/21/94	
503	Weight/Power Budgets (Included in CDRL 529)	9/15/94	
508	Acquisition Activities Plan	9/21/94	*
516	Instr. Interface Cont. Doc.	9/21/94	
521	Weekly Status Report	Weekly	
523	Performance Measurement Status Report (Included in CDRL 534)	9/22/94	
529	Reports of Work (Monthly Status Report)	9/15/94	
534	Mo./Qrtly. Financial Mgmt. Rpt. (NASA Fm. 533M/533Q)	9/22/94	
	*No submittal, no changes to CDRL.		

(continued)

Table XI EOS/AMSU-A September/October Documentation Planned Submittals (Cont.)

CDRL	Description	Due to NASA	Submitted to NASA
	October 1994:		
112	112 Worst Case Analysis	10/18/94	
203	203 Configuration Management Status Rpt (Included in CDRL 529)	10/14/94	
204	204 Performance Assurance Status (Included in CDRL 529)	10/14/94	
503	503 Weight/Power Budgets (Included in CDRL 529)	10/14/94	
521	521 Weekly Status Report	Weekly	
523	523 Performance Measurement Status Rpt (Included in CDRL 534)	10/21/94	
529	529 Reports of Work (Monthly Status Report)	10/14/94	
534	534 Mo./Qrtly. Financial Mgmt. Rpt. (NASA Fm. 533M/533Q)	10/21/94	
535	535 Subcontracting Report (Fm. 294)	10/31/94	
536	536 Summary Subcontracting Report (Fm. 295)	10/31/94	
None	None PAIP (Performance Assurance Implementation Plan)	10/12/94	

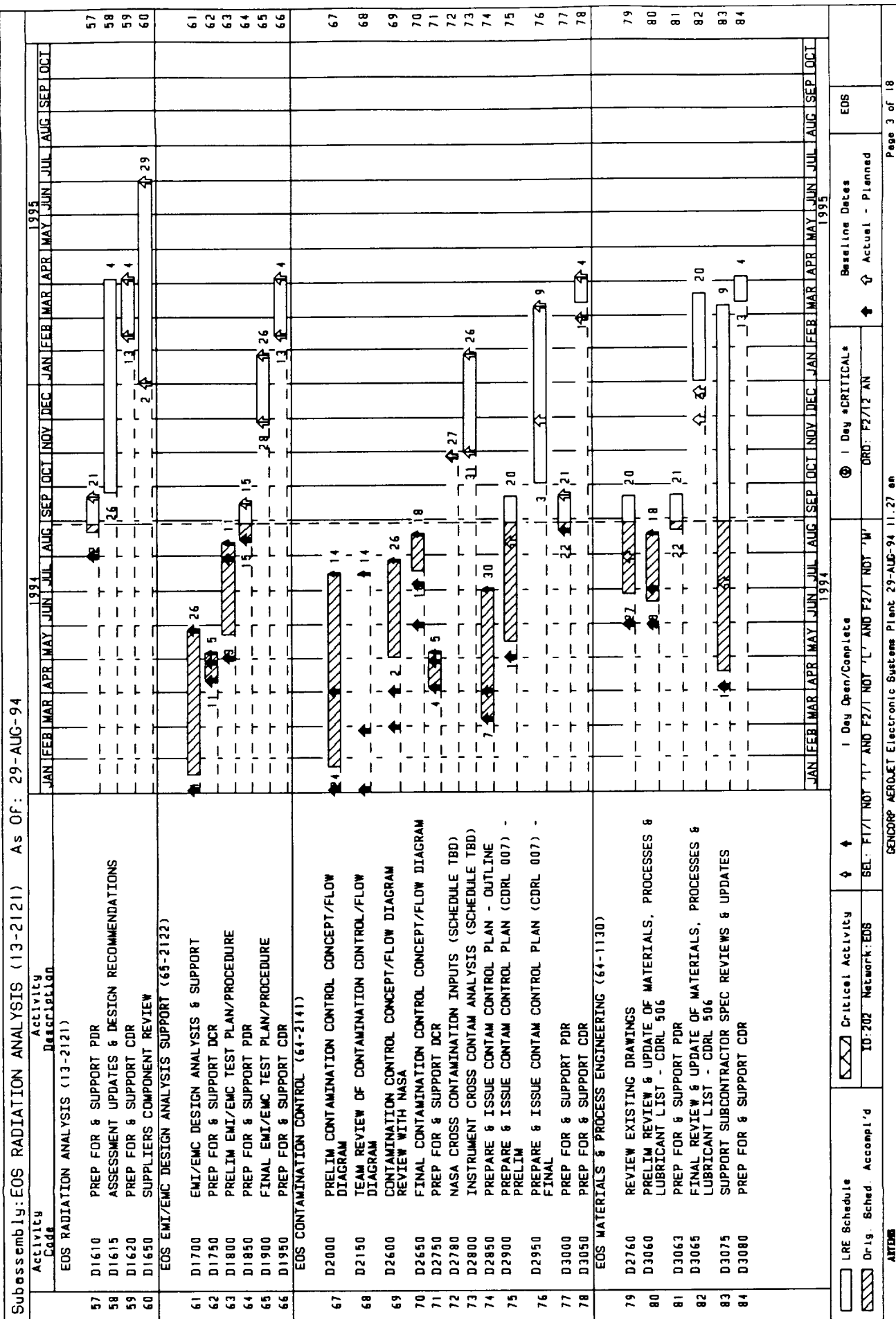
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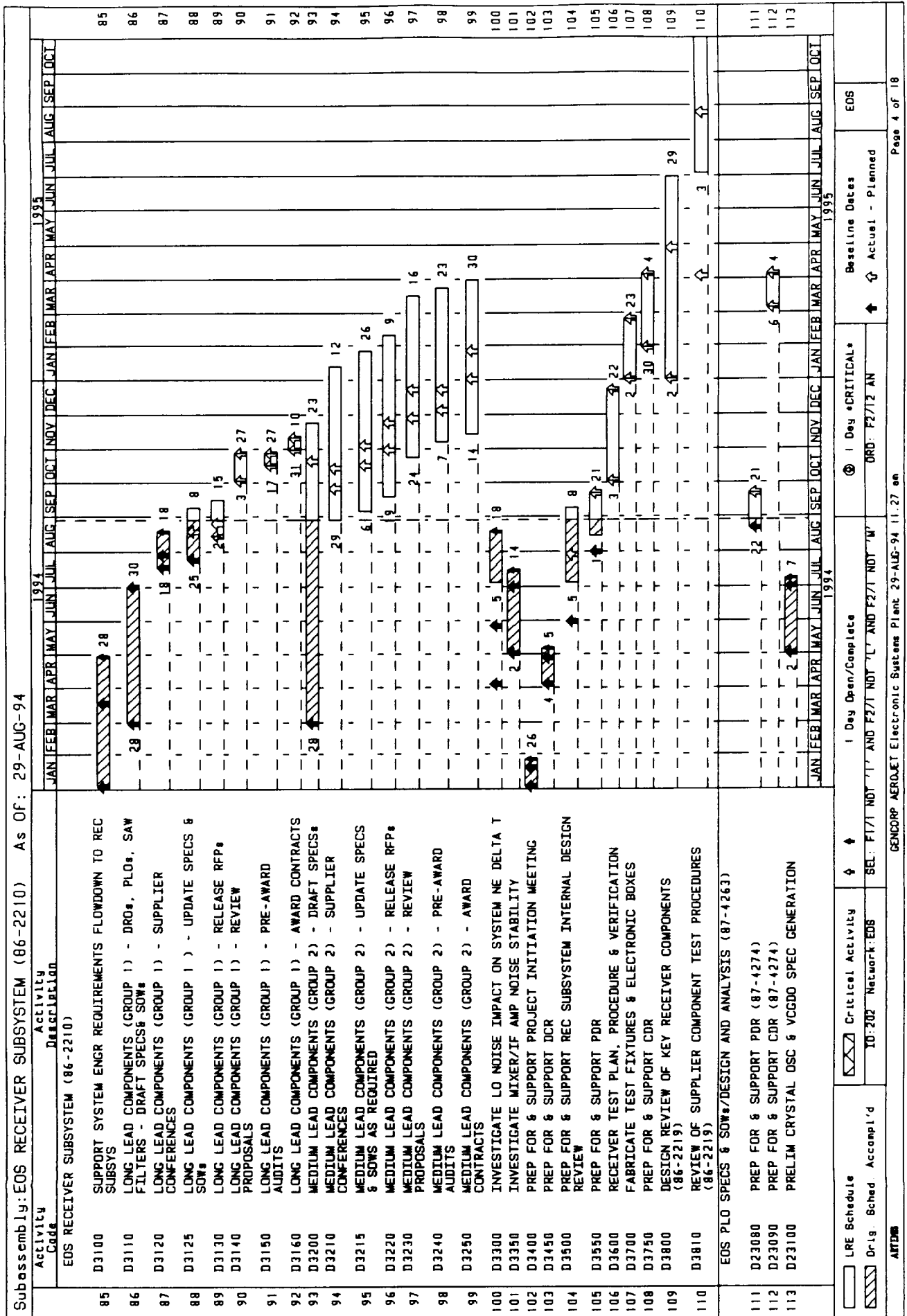
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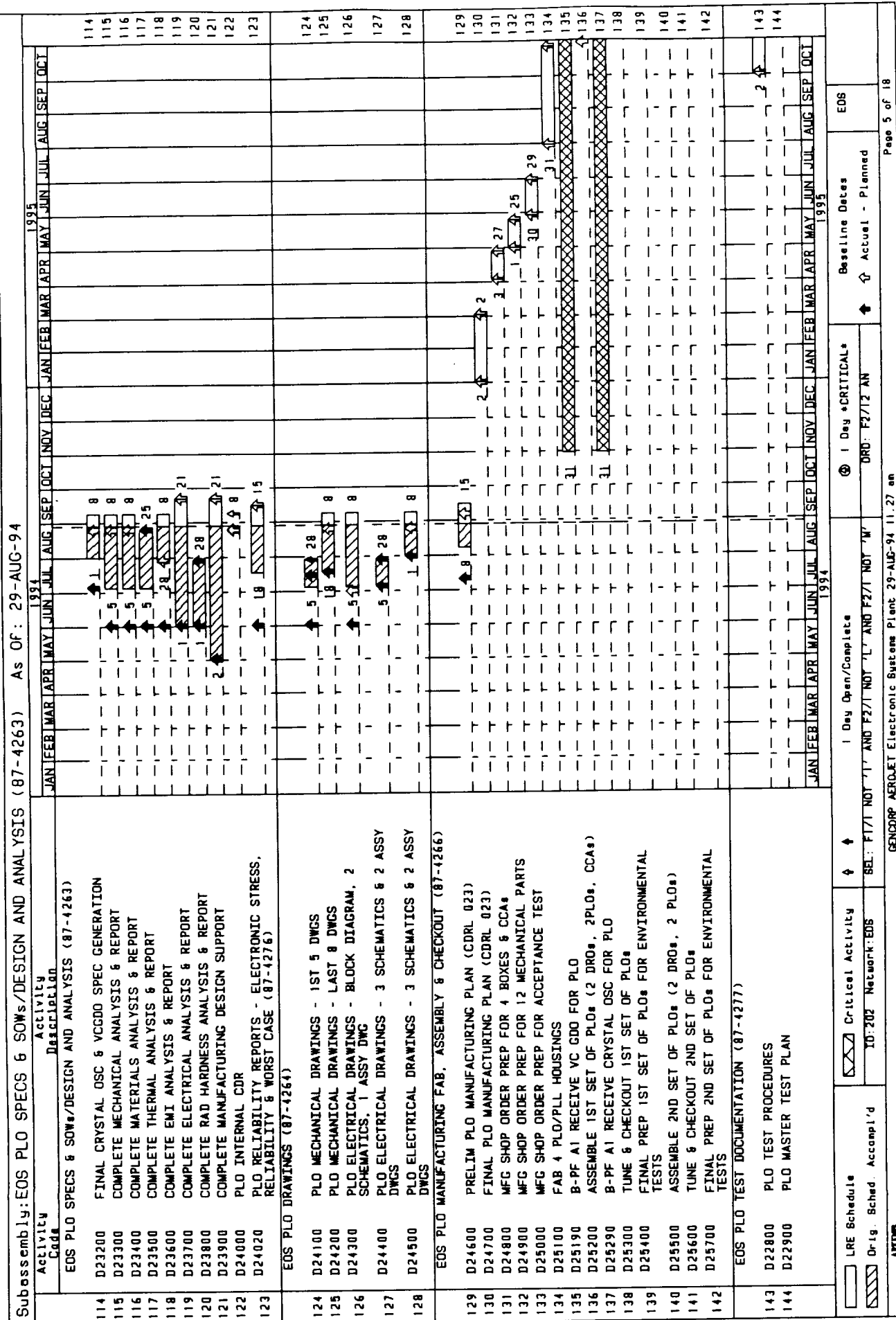
Contract modification six was issued 9 June 1994 and directed Aerojet to incorporate changes to update applicable documents identified in Section J (A-Statement of Work, C - Performance and Operation Specification, E - Contract Documentation Requirements List, G - General Interface Requirements Document, U - Unique Instrument Interface Document), revise the mission life requirement for the EOS AMSU-A instrument, and delete the requirement for a Bench Check Unit (reference Item A1, Clause B.1). Aerojet submitted price proposal C9180-80-02a on 28 July 1994. The proposal is now in the review cycle at GSFC.

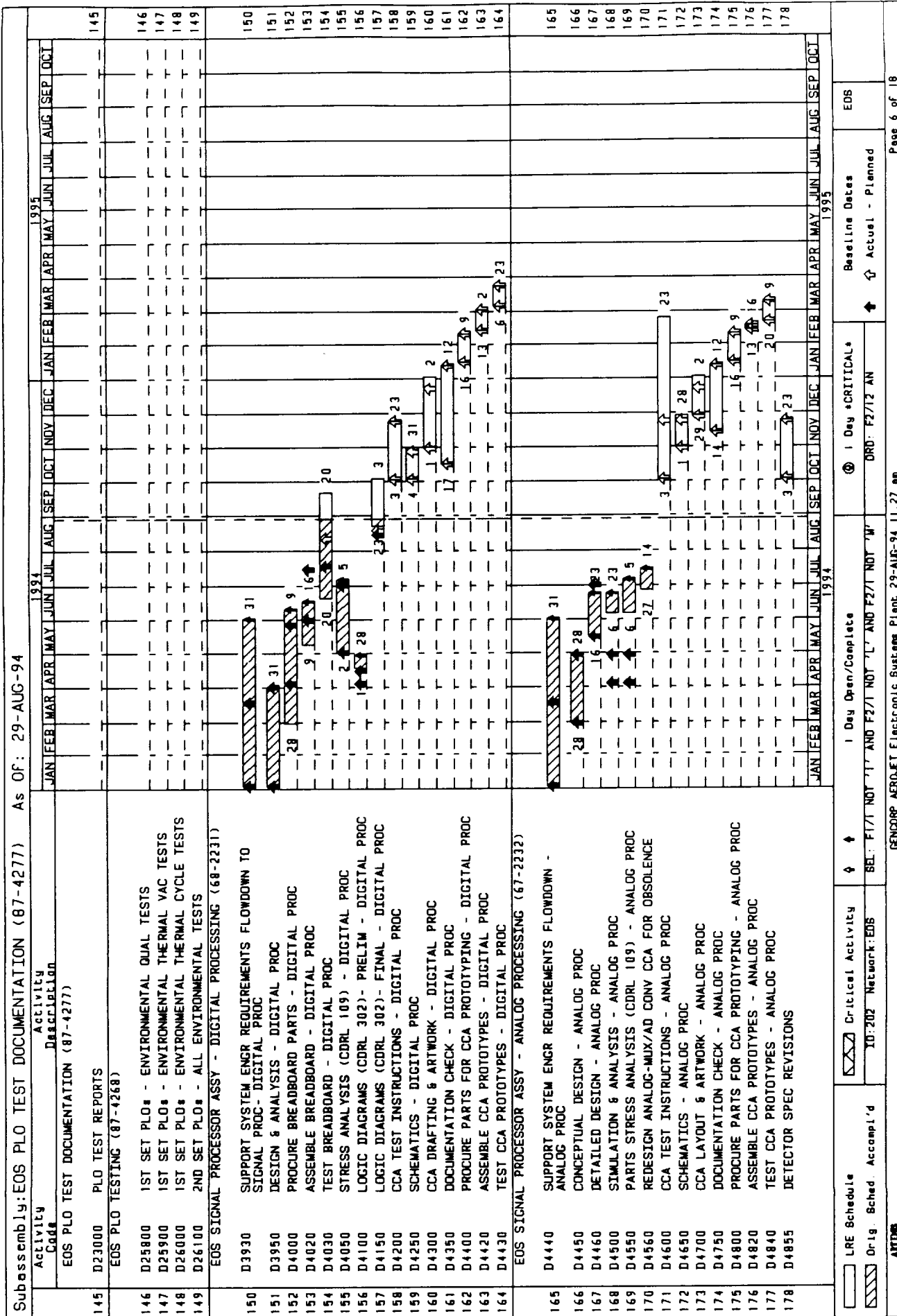
APPENDIX A

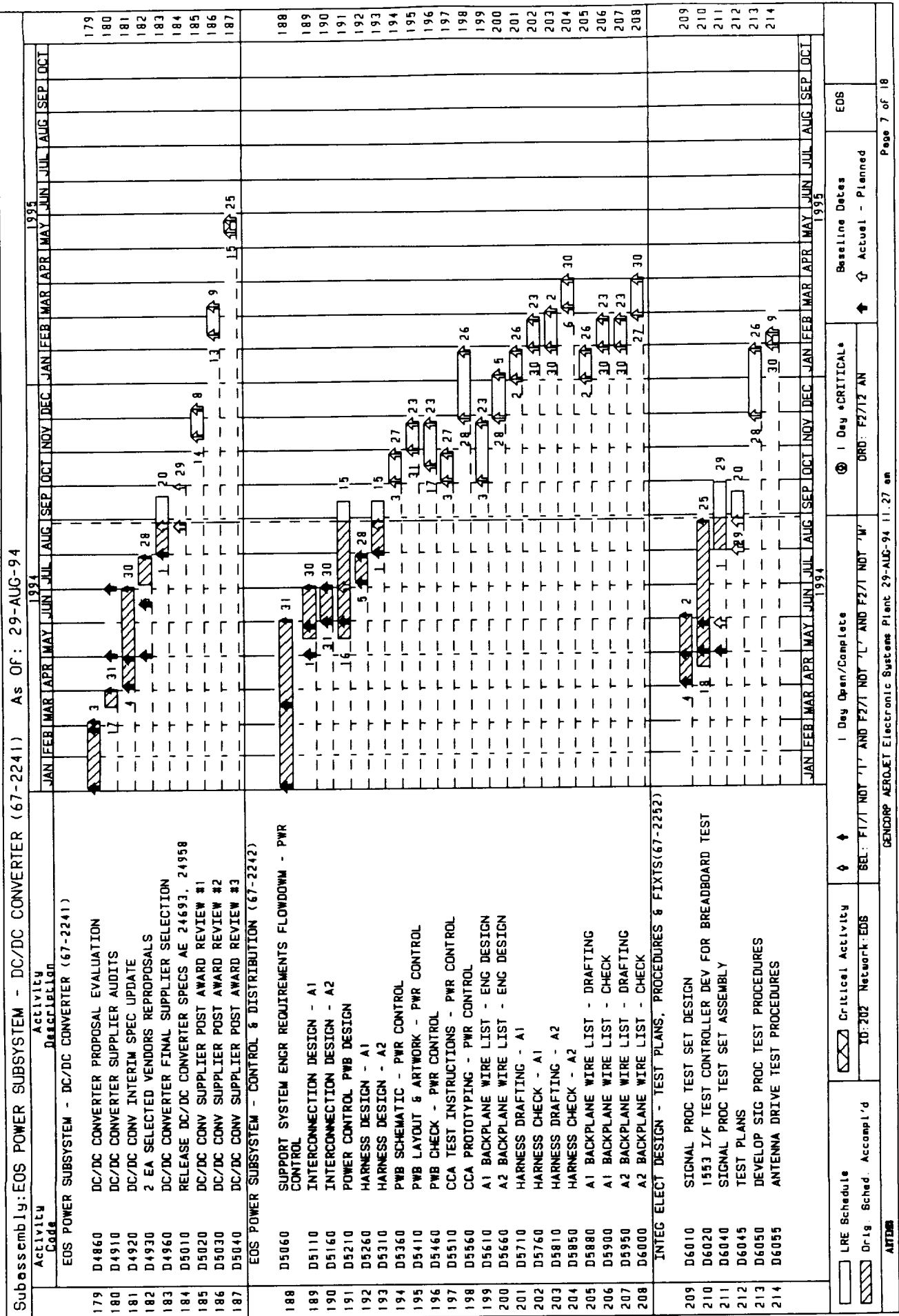
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SCHEDULES



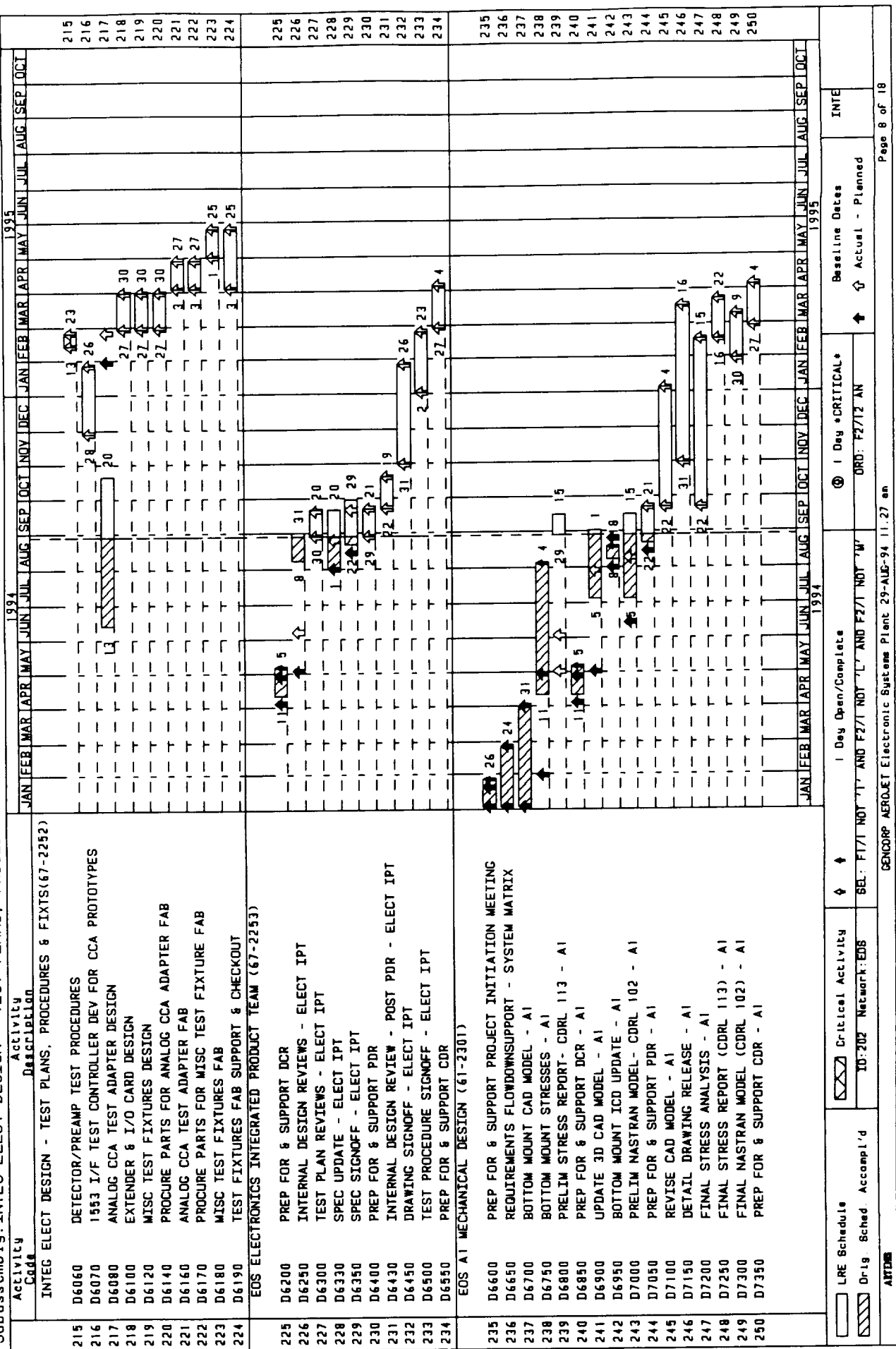








Subassembly: INTEG ELECT DESIGN - TEST PLANS, PROCEDURES & FIXTS(67-2252) As OF: 29-AUG-94

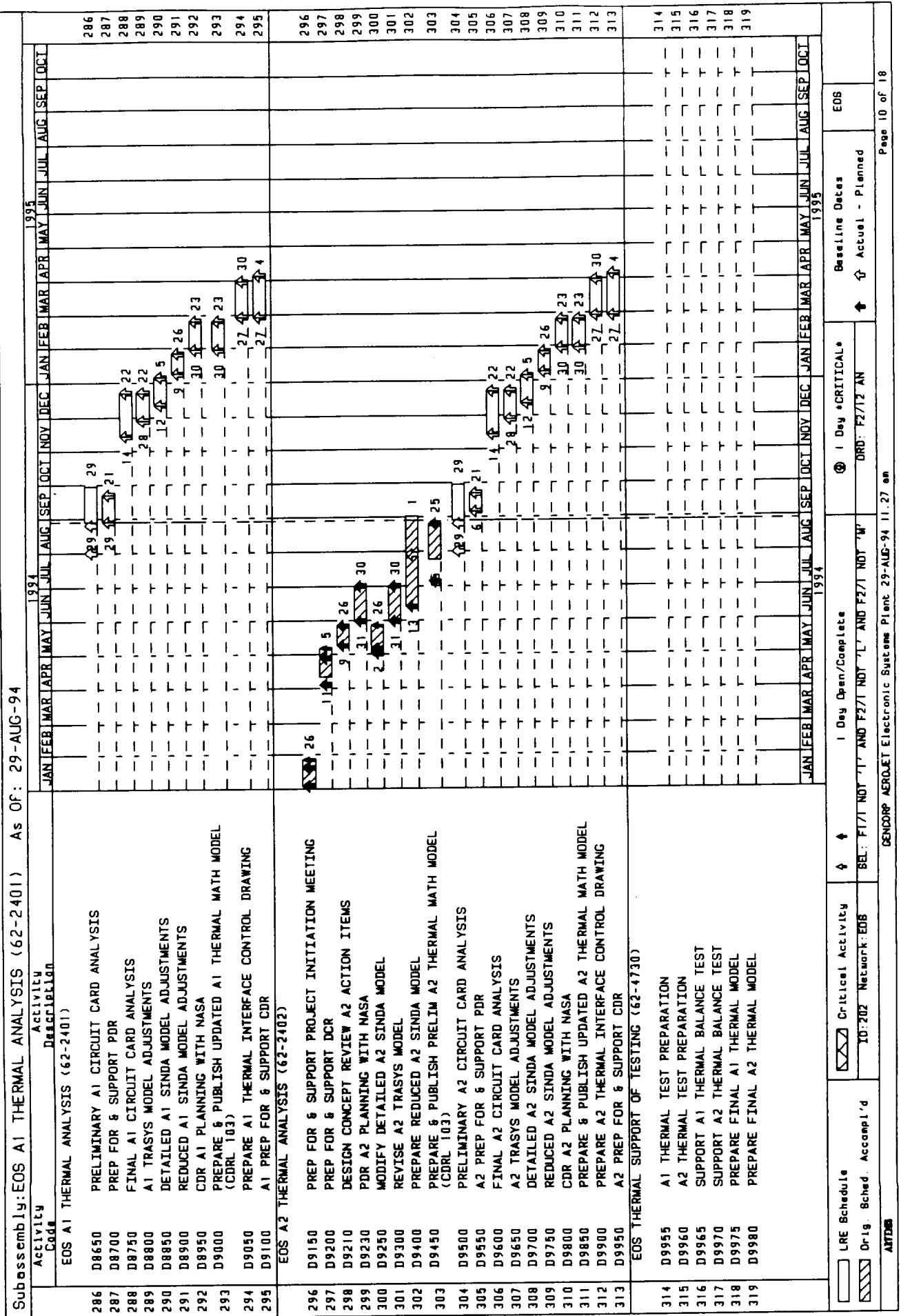


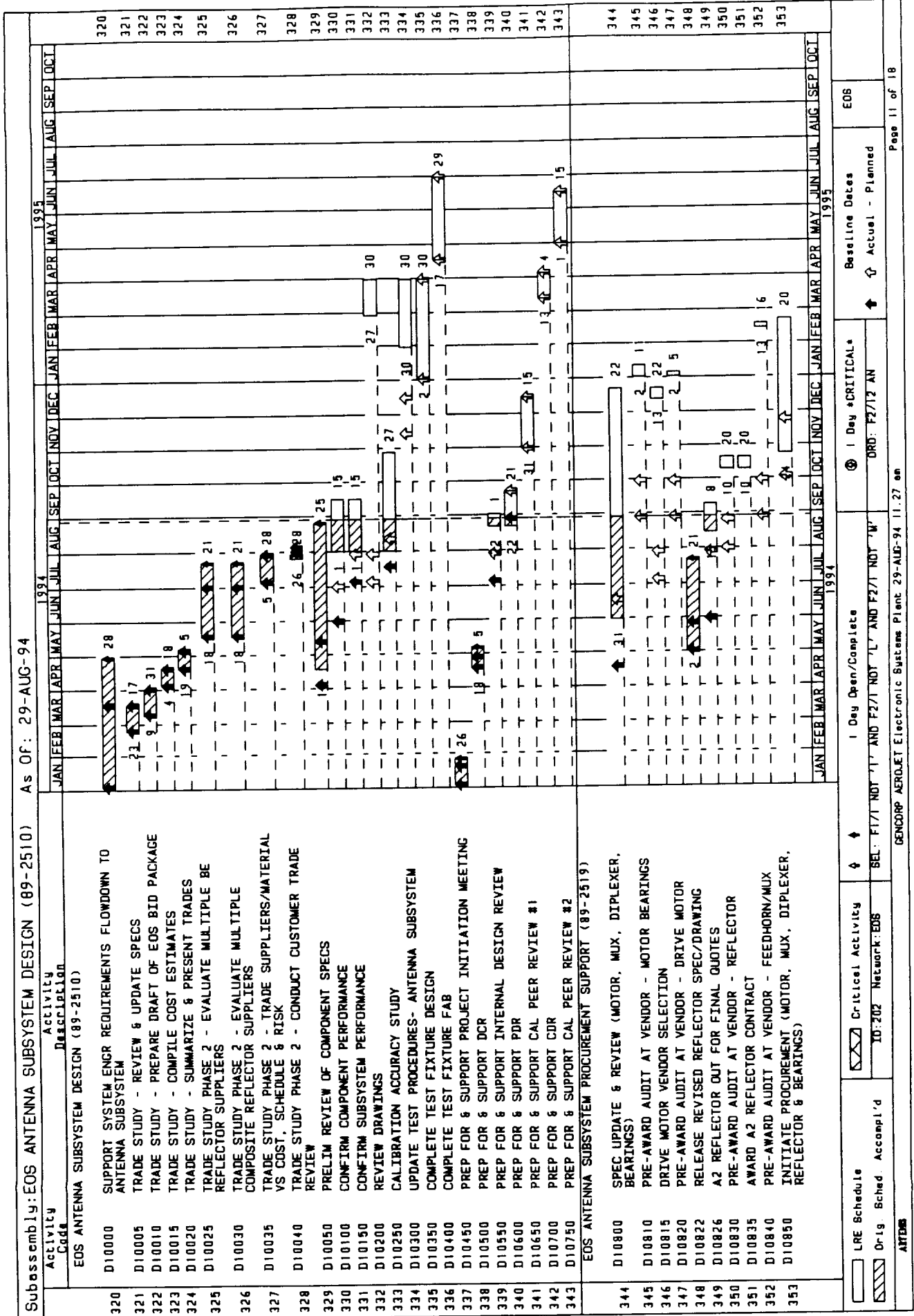
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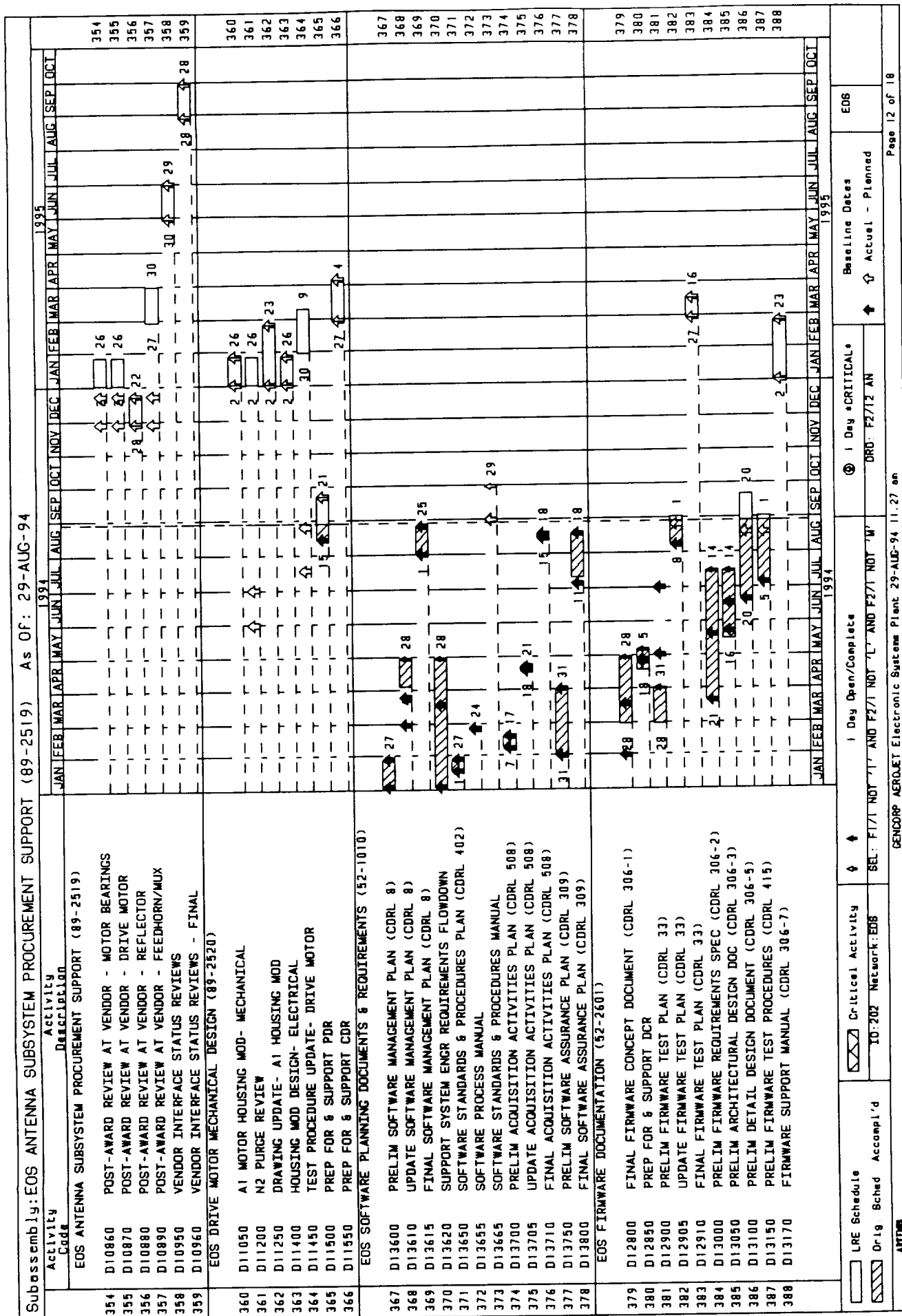
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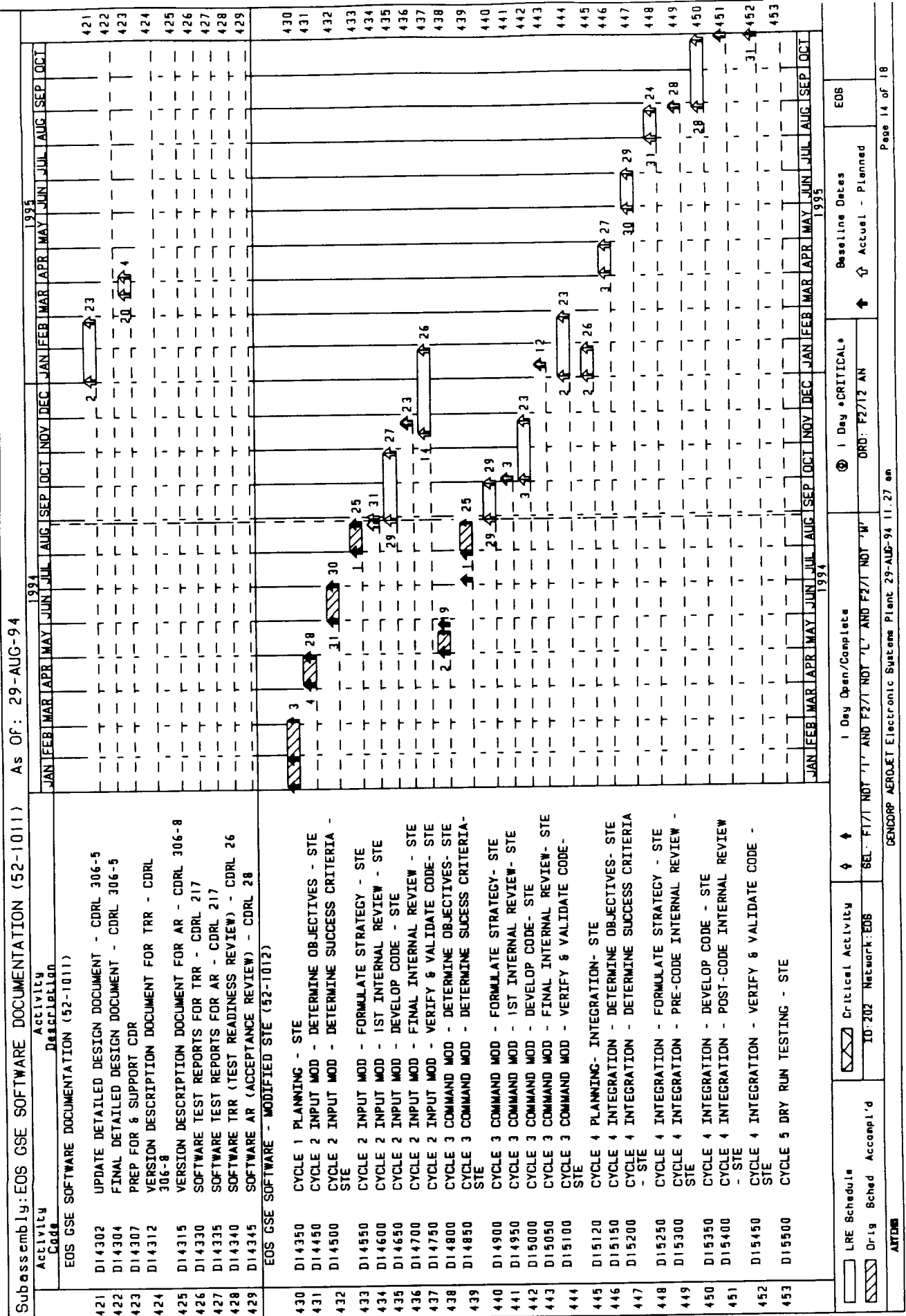
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Subassembly: EOS GSE SOFTWARE - MODIFIED STE (52-1012) As Of: 29-AUG-94												
Activity Code	Activity Description	1994										
		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV
454	EOS GSE SOFTWARE - MODIFIED STE (52-1012)											
455	EOS GSE SOFTWARE - FORMAL QUALIFICATION TESTING - STE											
456	EOS GSE SOFTWARE - SPACECRAFT CSTOL WORKSTATION (52-1013)											
457	CYCLE 1 PLANNING - CSTOL WS (INCL TRIP/TRAINING)											
458	CYCLE 2 MENU CONSTRUCTION - DETERMINE OBJECTIVES - CSTOL WS											
459	CYCLE 2 MENU CONSTRUCTION - DETERMINE SUCCESS CRITERIA - CSTOL WS											
460	CYCLE 2 MENU CONSTRUCTION - FORMULATE STRATEGY - CSTOL WS											
461	CYCLE 2 MENU CONSTRUCTION - 1ST INTERNAL REVIEW - CSTOL WS											
462	CYCLE 2 MENU CONSTRUCTION - DEV CODE - CSTOL WS											
463	CYCLE 2 MENU CONSTRUCTION - VERIFY & VALIDATE CODE - CSTOL WS											
464	CYCLE 2 MENU CONSTRUCTION - FINAL INTERNAL REVIEW - CSTOL WS											
465	CYCLE 3 INPUT TABLE DESIGN - DETERMINE OBJECTIVES - CSTOL WS											
466	CYCLE 3 INPUT TABLE DESIGN - DETERMINE SUCCESS CRITERIA - CSTOL WS											
467	CYCLE 3 INPUT TABLE DESIGN - FORMULATE STRATEGY - CSTOL WS											
468	CYCLE 3 INPUT TABLE DESIGN - 1ST INTERNAL REVIEW - CSTOL WS											
469	CYCLE 3 INPUT TABLE DESIGN - DEVELOP CODE - CSTOL WS											
470	CYCLE 3 INPUT TABLE DESIGN - VERIFY & VALIDATE CODE - CSTOL WS											
471	CYCLE 3 INPUT TABLE DESIGN - FINAL INTERNAL REVIEW - CSTOL WS											
472	CYCLE 4 PLANNING - INTEGRATION - CSTOL WS											
473	RECEIVE OASIS/CSTOL FROM COLORADO UNIV - SCHEDULE TBD											
474	CYCLE 4 INSTALL OASIS/CSTOL											
475	CYCLE 5 INTEGRATION - DETERMINE OBJECTIVES - CSTOL WS											
476	CYCLE 5 INTEGRATION - DETERMINE SUCCESS CRITERIA - CSTOL WS											
477	CYCLE 5 INTEG - FORMULATE STRATEGY - CSTOL WS											
478	CYCLE 5 INTEGRATION - PRE-CODE INTERNAL REVIEW - CSTOL WS											
479	CYCLE 5 INTEGRATION - DEVELOP CODE - CSTOL WS											
480	CYCLE 5 INTEGRATION - VERIFY & VALIDATE CODE - CSTOL WS											

A-14

A-16

Subassembly: EOS SYSTEMS ENGINEERING SPACECRAFT INTERFACE DESIGN(74-2130) As Of: 29-AUG-94

Activity Code	Activity Description	1994												1995											
		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT		
31	D940 PREP INTERFACE CONTROL DOC INPUT (CDRL 516) - 3RD UPDATE(DELIVER TO NASA)																								
32	EOS SYSTEMS ENGINEERING SPACECRAFT INTERFACE DESIGN(74-2130)																								
33	D950 PREP PERF VERIF PLAN (CDRL 022) & SPEC (CDRL 308) - PRELIM																								
34	D1000 PREP PERF VERIF PLAN (CDRL 022) & SPEC (CDRL 308) - PDR UPDATE																								
35	D1020 PREP PERF VERIFICATION PLAN (CDRL 022) & SPEC (CDRL 308) - FINAL																								
36	D1030 PREP PERF VERIFICATIONPROCEDURES (CDRL 412)																								
37	D1050 PREP CALIBRATION MANAGEMENT PLAN (CDRL 018) - PRELIM																								
38	D1100 PREP CALIBRATION MANAGEMENT PLAN (CDRL 018) - FINAL																								
39	D1120 PREP DETAILED GROUND CALIB PROCEDURES (CDRL 410)																								
40	D1150 PREP PRELIM OPERATIONAL IN-FLIGHT CHECKOUT PLAN (CDRL 025)																								
41	D1180 PREP FINAL OPERATIONAL IN-FLIGHT CHECK-OUT PLAN																								
42	D1200 PREP OPERATIONAL IN-FLIGHT CALIB PROCEDURE (CDRL 404) - PRELIM																								
43	D1250 PREP GEN. OPERATIONAL COMMAND PROCEDURE (CDRL 405) - PRELIM																								
44	D1260 PREP CONTROL OF UNSCHEDULED ACTIVITIES (CDRL 516)																								
45	D1270 PREP STORAGE PLANS (CDRL 24)																								
46	D1280 PREP TRANSPORTATION & HANDLING PROCEDURES (CDRL 406)																								
47	D1290 PREP ASSEMBLY PROCEDURES (CDRL 413)																								
48	D1295 PREP DETAILED TEST PROCEDURES (CDRL 409)																								
49	EOS SYSTEMS ENGINEERING MEETING SUPPORT (74-2160)																								
50	D1300 PREP FOR & SUPPORT DCR																								
51	D1350 PREP FOR & SUPPORT PDR																								
52	D1360 PREP FOR & SUPPORT CPR 1																								
53	D1380 PREP FOR & SUPPORT CDR																								
54	EOS SPARES DEFINITION (74-1410)																								
55	D1400 PREP SPARES PROGRAM PLAN (CDRL 035) - PRELIM																								
56	D1450 PREP SPARES PROGRAM PLAN (CDRL 035) - FINAL																								
57	EOS RADIATION ANALYSIS (13-2121)																								
58	D1500 PRELIM DATA BASE SEARCHES																								
59	D1550 PRELIM SHIELDING ANALYSIS/DESIGN CRITERIA MEMO																								
60	D1600 PRELIM PARTS ASSESSMENT & DCR SUPPORT																								

LRE Schedule

Or-Ig. Sched

Critical Activity

Accompl'd

10-202 Network:EOS

SEL: F1/T1 NOT "1" AND F2/T1 NOT "1" AND F2/T1 NOT "M"

1 Day Open/Complete

1 Day *CRITICAL*

Baseline Dates

Actual - Planned

EOS

1995

Page 2 of 18

GENCORP AEROLJET Electronic Systems Plant 29-AUG-94 11:27 am

APPENDIX B

ACTION ITEM RESPONSES

ACTION ITEM RESPONSE

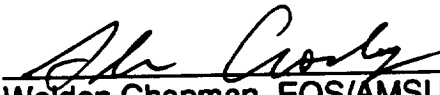
ACTION ITEM NO. 7/26-1

ACTION REQUESTED:

Spacecraft System Concept Review is planned for end of 1995. Aerojet should aim to start working ICD issues with spacecraft contractor starting two months after the scheduled award date of July '95. Final ICDs should be available at the SCR. Put this in ARTEMIS/PMS planning.

RESPONSE:

Compliance with this action item has been accomplished by shifting a milestone date of task 01 of account 4170-74-2130 from June '95 to Dec '95 in the PMS and by shifting milestones of ICD submittals in task 04 of account 4170-74-2130. (See also Action Item No. 7/26-3.) PMS has been updated, and ARTEMIS will reflect this update in the next revision.

for 
Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader

8/11/94
Date

ACTION ITEM RESPONSE

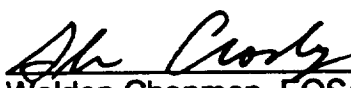
ACTION ITEM NO. 7/26-3

ACTION REQUESTED:

System engineering schedule status (page 33). Add updates to ICD plan to post-PDR, post-CDR (if required) and the August-December '95 time frame for coordination with the spacecraft contractor (see AI 7/26-1) above).

RESPONSE:

Compliance with this action item has been accomplished by shifting a milestone date of task 01 of account 4170-74-2130 from June '95 to Dec '95 in the PMS and by shifting milestones of ICD submittals in task 04 of account 4170-74-2130. (See also Action Item No. 7.26-1.) PMS has been updated, and ARTEMIS will reflect this update in the next revision.

for 
Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader

8/11/94
Date

ACTION ITEM RESPONSE

ACTION ITEM NO: 7/26-4

ACTION REQUESTED:

Provide data for COI bond line stress levels for launch loads.

RESPONSE:

COI has responded with Attachment 1 that gives the maximum stress of 30 psi. The 90 g load is the qualification load that was derived by Aerojet from NOAA A2 random vibration test measurements. It is the equivalent to the worst case launch loading environment.

It should be noted that this is very preliminary information. A final vendor for the A2 composite reflector has yet to be chosen.



Wayne Ely, Team Leader
Mechanical/Thermal Subsystem



Attachment 1

page 1 of 1

EOS/AMSV-A A2 Reflector Assembly Preliminary Fitting Bond Analysis

- From COI Proposal #PL-1213, Figure 2.2.2.1 the approximate fitting to parabolic shell bond area = 2.6 in^2
- Per section 2.3.2 the weight of the assembly (not including fitting) is .87 lb.
- Per Aerjet assembly must withstand 90G loading
 - Fitting Bond must react $(90G)(.87 \text{ lb}) = 78.3 \text{ lb}$
 - As worst case assume bond is normal to bond, resulting in bond tension.
 - Bond stress = $\frac{P}{A} = \frac{78.3 \text{ lb}}{2.6 \text{ in}^2} = \underline{\underline{30 \text{ psi}}}$
 - Typical Bond allowable is 1000 psi
 - Margin (with SF of 1.5) = $\frac{1000}{(1.5)(30)} - 1 = \underline{\underline{21}} \checkmark$

August 9, 1994

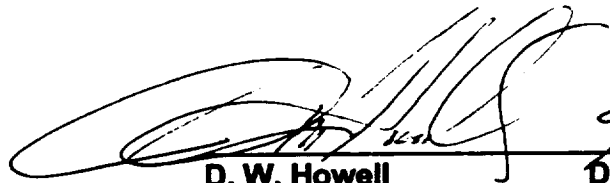
*FED X PRESSED
To M. Domini 8/10/94*

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/26-7

DESCRIPTION: Provide NASA a copy of the A2 reflector specification including envelope drawing.

RESPONSE: A copy of the A-2 Reflector Assembly Specification (AE-26582) and envelope drawing (dwg. #1355835) are enclosed.


D. W. Howell
Program Manager
EOS/AMSU-A Program

8/10/94
Date

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/26-10

ACTION REQUESTED:

Antenna motor bearings - define what is meant by "bake-out" on page 92

RESPONSE:

The reference to bake out is made regarding the bearing cleaning and lubrication process as specified in Aerojet specification No. AE-26060, entitled "Inspection, Cleaning, and Lubrication Procedures for Ball Bearings and Lubricant Reservoirs - AMSU-A." (This specification has been provided to the EOS/AMSU-A Technical Officer.)

There are numerous bake-out procedures specified in the specification for both cleaning and lubrication of bearing parts. The significant ones regarding outgassing are administered after introduction of the lubricant. Four such procedures were identified.

Three different bake-out procedures are specified for vacuum impregnation of the Apiezon C lubricant into various porous parts used in the assembly: machinable, microporous elastomer and polyimide materials and phenolic retainers. These processes generally call for oil impregnation at 10^{-4} torr and 150°F (65.6°C) and maintenance of these conditions for one hour after impregnation (see AE-26060 for details).

The final bake-out procedure involves the completed bearing assembly, already containing lubricant-impregnated parts. The assembly is immersed in the lubricant at conditions of 10^{-4} torr and 150°F and maintained for two hours. The vacuum is then broken and the lubricated bearings maintained at 150°F for six days.

Specification AE-26060 was prepared for the NOAA/AMSU-A program to ensure clean and well-lubricated bearings. The bake-outs were intended for this purpose and not as an outgassing procedure. The specification will be reviewed to see if it can be appropriately modified to include bake-outs for outgassing elimination after results by GSFC regarding the Apiezon C sample outgassing characteristics are obtained

for *Weldon Chapman*
Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader

8/9/94
Date

Harold Cover
Harold Cover, EOS/AMSU-A
Contamination, Materials, and
Processes Team Leader

8/9/94
Date

ACTION ITEM RESPONSE

ATTACHMENT 4

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/26-18

ACTION REQUESTED:

Provide radiation study/analysis that established EOS requirements and how these requirements are to be met. If shielding is to be used provide type, size thickness, etc. of shielding. Explain how the radiation requirements of the GIRD and PAR were/are met. (Also see AI 7/26-9.)

RESPONSE:

The radiation study/analysis that established EOS requirements is documented in the attached memo by Jim Parkinson. It has been reviewed, and no update is required. A conference call will be scheduled between Jim Parkinson and Bob Shelley/Mark Domen after this memo submittal is reviewed. (See Action Item 7/26-9.) Close out of this action item will be accomplished at PDR.

For 
Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader

8/11/94
Date

Radiation Survivability Guide and Specification (EOS/AMSU)

All subsystems must be capable of surviving five years in a 705-Km circular near-polar ($i = 98^\circ$) orbit.

Electronic devices in ceramic flatpacks or standard kovar cans which are survivable to 10^5 Krad(Si) total dose, and are not subject to single-event phenomena, may be used in this program without special shielding. Otherwise, see below.

Total Dose

The doses which may be expected under various conditions of shielding are as given below:

Condition	Exposure	Total Dose (5-years)	Dose with x2 Margin
A.	Satellite surface materials	$\sim 10^4$ Krad	$\sim 2 \times 10^4$ Krad
B.	Si chip in 0.22 gm/cm^2 package	50 Krad	100 Krad
C.	Si chip within instrument structure	27 Krad	54 Krad
D.	Si chip in package and structure	16 Krad	31 Krad
E.	Si chip in package, 60 mil Al box, structure	6 Krad	12 Krad
F.	Si chip behind heavy shielding	~ 2 Krad	~ 5 Krad

A design margin of x10 is desired, and x2 is absolutely required. (Definitive radiation data is required for use of a design margin as low as 2.)

Many power transistors and integrated circuits are not reliably survivable to 270 Krad, or even to 54 Krad. Therefore, the subcontractor may prefer to take advantage of the box structure around the electronics (as measured by the thinnest shielding in each direction; i.e., a 100-mil wall hogged out to 40-mils over 40% of its area nevertheless provides only 40-mils of effective shielding).

If the subcontractor's box walls are aluminum and provide a minimum of "x" thickness (" ρx " gm/cm^2 areal density), then the 5-year dose inside the box will be approximately

$$D = \frac{27}{\left[1 + \frac{x}{x_0}\right]^{1.5}} = \frac{27}{\left[1 + \frac{\rho x}{\rho x_0}\right]^{1.5}} \text{ Krad(Si)} \quad (1)$$

where $\rho x_0 = 0.35 \text{ gm/cm}^2$, or $x_0 = 51$ mil. (Beyond 1.7 gm/cm^2 the dose is only proportional to x^{-1} .)

If another material is substituted for aluminum, it may not be equally effective. For elements of atomic number $z \leq 14$ (e.g., silicon, magnesium, alumina, glass, and most organics), they may be substituted as gm/cm^2 on a one-for-one basis. (E.g., 0.15cm of $\rho = 2.7\text{gm/cm}^3$ Al is equivalent to 0.2334 cm of $\rho = 1.74\text{gm/cm}^3$ Mg; both have $\rho = 0.405\text{gm/cm}^2$ areal density.) For heavier elements ($z > 14$) the effective areal density must be reduced by a factor of $[(z+3)/16]^{-0.34}$. E.g., 0.1cm of $\rho = 8.96\text{gm/cm}^3$ copper is equivalent to aluminum of

$$\rho x|_{Al} = 0.1(8.96)[(29+3)/16]^{-0.34} = 0.708\text{gm/cm}^2 (= 0.26\text{cm Al}) \quad (2)$$

which means copper is 21% less efficient than the same weight aluminum. [Nevertheless, 0.1cm of copper is 62% thinner than the equivalent aluminum.]

Protons

Although the ionizing effects of solar and trapped protons are included in total dose (above), protons and heavier ions also produce displacement damage. Proton fluxes are expected in the range 10^{10} - 10^{11} p/cm^2 . Survivability of an electronic part to 10^{12}n/cm^2 may be considered adequate evidence of survivability against protons.

Single Event Phenomena (Transient and Permanent Upsets, Latchup, Burnout)

Single-event cross sections are measured in $\text{cm}^2/\text{particle}$ for a given dE/dx , called linear energy transfer ("LET") in $\text{MeV-cm}^2/\text{mg}$. The mean long-term-averaged cosmic-ray particle rate may be approximated as

$$\phi \approx 50 / \text{LET}^{2.5} \text{ particle / cm}^2\text{-day} \quad (3a)$$

$$(\text{LET} < 25 \text{ MeV-cm}^2/\text{gm})$$

and

$$\phi \approx 0.02 / (\text{LET} / 20)^8 \text{ particle/cm}^2\text{-day} \quad (3b)$$

$$(\text{LET} > 20 \text{ MeV-cm}^2/\text{gm})$$

Single-event upset (SEU) rates will usually be acceptable if the device cross section is $\leq 10^{-8}\text{cm}^2/\text{particle}$, or $< 10^{-6}$ error/device-day (error/bit-day in ROMS and RAMS must be much smaller to keep the per-device error rate negligible).

Occurrence of single-event latchup (SEL) is an indication not to use the device. (In an extreme case of no alternative part, a latchup-detect/reset circuit would need to be provided. If such a part is contemplated, the prime contractor [Aerojet] should be notified immediately.)

Single-event burnout (SEB) may be a problem in some power transistors, including bipolar power transistors. SEB is not permissible. (It may usually be avoided by designing with voltages $\leq 75\%$ of the breakdown voltage, or $\leq 25\%$ for Darlington pairs.)

Shortfalls

The subcontractor shall furnish Aerojet a list of the electronic parts to be used, or contemplated to be used. The list shall consist of three categories: [1] Parts which are adequately survivable (furnish survivability levels for each), [2] Parts with design margins between $\times 2$ and $\times 10$, and [3] Parts with incompletely-known survivability. Parts sensitive to ≤ 5 Krads should not be used. [The subcontractor may ask Aerojet assistance for survivability information.]

August 10, 1994

*FAVED TO
M. Domen 8/10/94*

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/26-21

DESCRIPTION:

Provide list of schedule "Critical" parts and materials ASAP for expediting by GSFC.
Submit NSPARs at least 30 days prior to procurement date.

Background: The intent of this action item was to identify which NSPARs need GSFC review on a priority basis.

RESPONSE:

The most "critical" parts are those used in the following components/subassemblies:

<u>ITEM</u>	<u>COMPONENT</u>	<u>SUPPLIER</u>
1.	VCGDO	Litton
2.	TCXO	FEI
3.	DC/DC Converter	TBD
4.	1553 Microcircuit	DDC
5.	DRO	Litton
6.	Saw Filter	Phonon
7.	Mixer/Amplifiers	Spacek
8.	IF Amplifiers	Amplica
9.	Motors	Magtech (Vernitron)

Items 1, 2 and 3 on the above list are new components and/or new vendors and data is not yet available for Aerojet or NASA review. However, when available, this data will be expeditiously submitted and should receive priority review.

Item 4, the 1553 microcircuit is also new, but the GSFC FAM (R. Shelley) participated in July 28, 1994 supplier discussions regarding these parts and is already working the associated issues. A specification has been drafted and after input into the proper format, a copy will be submitted for Mr. Shelley's review and comment.

Based on the above, the NSPARs that currently need priority attention are those listed in the EOS/AMSU subcontractor Preliminary Parts List* under the (hereto attached) sections for Litton, Spacek, Amplica and Magtech. Phonon is not included because no NSPARs were generated for Phonon on NOAA. Please note the NSPAR numbers which have been circled on the attached sections are the NOAA-generated NSPARs which are not required on EOS because the parts are Grade 1 or 2 and listed in either PPL 20 or MIL-STD-975, and therefore review/approval by GSFC is not necessary.

*The EOS/AMSU subcontractor Preliminary Parts List is based on the NOAA/AMSU-A PDIL.


Emil Lorenz 8/10/94
Date

EOS/AMSU SUBCONTRACTOR PRELIMINARY PARTS LIST

LITTON

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART NUMBER	QTY PER SYS	NSPAR NUMBER	GSFC NSPAR STATUS	DPA STATUS CODE	DATE
CABLE, RF, COAX, .085 SEMIRIGID	1205665	1205665		M17/133-RG405	1	L157	APPROV		
CABLE, RF, COAX, .141 SEMIRIGID	1205571	1205571		M17/130-RG402	1	L155	CANCEL		
CONNECTOR, RIGHT ANGLE, SMA	1205381	1205381			1	L152	APPROV		
Connector, SMA Plug	2248	2248		M39012/60-3002	1	L165	APPROV		
CONNECTOR, SMA PLUG, SEMIRIGID	1205570	1205570		M39012/79-3102	1	L154	CANCEL		
CONNECTOR, SMA PLUG, SEMIRIGID	1205655	1205655		M39012/79-3001	1	L158	APPROV		
DIODE, RECTIFIER, SCHOTTKY	1205363-00	1205363			1	L144	APPROV		
DIODE, VARACTOR, GaAs MULT.	30059	30059			1	L1518	APPROV		
DIODE, ZENER	1205373-04, -05, -06	1205373			1	L148	APPROV		
DRO FINAL ASSEMBLY	1205581-01 THRU -05	1205581			1	L156	APPROV		
FILTER, EMI, HERMETIC SEAL	1200512	1200512		M28861/05-0061B	1	L153	APPROV		
INDUCTOR	1205397	1205397			1	L149A	APPROV		
LOW PASS EMI FILTER FEEDTHRU	30060	30060			1	L150	CANCEL		
MCXT., REG., ADJUSTABLE, 1A	1205364-00	1205364			1	L147A	APPROV		
MCXT., REG., SWITCHING, 1.25A	1205357-01	1205357			1	L141	CANCEL		
MCXT., REG., SWITCHING, 2.5A	1205358-01	1205358			1	L142	CANCEL		
MCXT., REG., SWITCHING, 5.0A	1205359-01	1205359			1	L143B	APPROV		
RF ISOLATOR	1205334-01 THRU -05	1205334			1	L146	APPROV		
VARACTOR TRIPLER	1205333-01 THRU -05	1205333			1	L145	CANCEL		

DPA STATUS CODE: A=ACCEPTABLE, I=IN REVIEW, R=PARTS/LOT REJECTED,
U=REPORT UNACCEPTABLE, BLANK=NOT RECEIVED,
N/A=NOT APPLICABLE, N/R=NOT REQUIRED

EOS/MSU SUBCONTRACTOR PRELIMINARY PARTS LIST

SPACEK

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART NUMBER	QTY	NSPAR NUMBER	GSFC NSPAR NUMBER	DPA STATUS	DATE
					PER				
					SYS				
CAPACITOR, CHIP	200A103NP50	30021	ATC			SP084-01B	CONCUR	A	8847
CAPACITOR, CHIP	200A502NP50	30021	ATC			SP084-02B	CONCUR	A	8913
CAPACITOR, CHIP	200B104NP50	30021	ATC			SP084-03B	CONCUR	A	8847
CAPACITOR, CHIP	CDR128G150AJUM	MIL-C-55681/4	ATC	100A150JPH		SP085-01B	CONCUR	N/R	8810
CAPACITOR, CHIP	CDR128G180ACUM	MIL-C-55681/4	ATC	100A180CPH		SP085-02B	CONCUR	N/R	8906
CAPACITOR, CHIP	CDR128G188ACUM	MIL-C-55681/4	ATC	100A188CPH		SP085-03B	CONCUR	N/R	8828
CAPACITOR, CHIP	CDR128G2R2ACUM	MIL-C-55681/4	ATC	100A2R2CPH		SP085-04B	CONCUR	N/R	8821
CAPACITOR, CHIP	CDR128G2R4ACUM	MIL-C-55681/4	ATC	100A2R4CPH		SP085-05B	CONCUR	N/R	8832
CAPACITOR, CHIP	CDR128G2R4ACUM	MIL-C-55681/4	ATC	100A2R4CPH		SP085-05B	CONCUR	N/R	8840
CAPACITOR, CHIP	CDR128G2R7ACUM	MIL-C-55681/4	ATC	100A2R7CPH		SP085-06B	CONCUR	N/R	8750
CAPACITOR, CHIP	CDR128G2R7ACUM	MIL-C-55681/4	ATC	100A2R7CPH		SP085-06B	CONCUR	N/R	8815
CAPACITOR, CHIP	CDR128G3R3ACUM	MIL-C-55681/4	ATC	100A3R3CPH		SP085-07B	CONCUR	N/R	8750
CAPACITOR, CHIP	CDR128G510AJUM	MIL-C-55681/4	ATC	100A510JPH		SP085-08B	CONCUR	N/R	8836
CAPACITOR, CHIP	CDR128G560AJUM	MIL-C-55681/4	ATC	100A560JPH		SP085-09B	CONCUR	N/R	8819
CAPACITOR, CHIP	CDR128G6R2ACUS	MIL-C-55681/4	ATC	100A6R2CPH		SP085-11B	CONCUR	N/R	8823
CAPACITOR, CHIP	CDR128G8R2AJUM	MIL-C-55681/4	ATC	100A8R2JPH		SP085-10B	CONCUR	N/R	8828
CONNECTOR, SMA	2052-3357-02		OMNI-SPECTRA		1	SP119	CONCUR	A	8938
DIODE	JANS1M647-1	MIL-S-19500/240	MICROSEMI	1N647-1	1	STD	N/R	N/A	8752
DIODE, SCHOTTKY, MIXER	MD915	30008	I.I.	MD654	2	SP100	CONCUR	A	A8906
DIODE, SCHOTTKY, MIXER	MD915	30008	I.I.	MD654	2	SP100	CONCUR	A	A8840
FILTER, FEED-THRU	M15733/44-0002	MIL-F-15733/44	MURATA ERIE	1250-063	1	SP083C	CONCUR	A	8810A
HYBRID, AMPLIFIER	30018-1	30018	COUGAR COMP.	AC457A (-1 TO -9)	1	SP104-01B	CONCUR	A/P	8923
HYBRID, AMPLIFIER	30018-2	30018	COUGAR COMP.	AC434-4A (-1 TO -9)	1	SP104-02B	CONCUR	A	8923
HYBRID, RF AMPLIFIER	A29-2P	30019	WJ	A28-2 (-10)	3	SP080A	CONCUR	A/P	8846
RESISTOR, CHIP	M55342K06R150JS	MIL-R-55342/6	STATE OF THE ART	RM0705		SP086-01	CONCUR	A	8728

DPA STATUS CODE: A=ACCEPTABLE, I=IN REVIEW, R=PARTS/LOT REJECTED,
U=REPORT UNACCEPTABLE, BLANK=NOT RECEIVED,
N/A=NOT APPLICABLE, N/R=NOT REQUIRED

EOS/AMSU SUBCONTRACTOR PRELIMINARY PARTS LIST

SPACEK

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR		QTY	NSPAR		GSFC	DATE	
				MIL-SPEC PART NUMBER	NUMBER		PER	NUMBER		NSPAR	STATUS CODE
RESISTOR, CHIP	M55342K06R220JS	MIL-R-55342/6	STATE OF THE ART	RH0705						CONCUR A	8923
RESISTOR, CHIP	M55342K06R330JS	MIL-R-55342/6	STATE OF THE ART	RH0705						CONCUR A	8831
RESISTOR, CHIP	M55342K06R3K30S	MIL-R-55342/6	STATE OF THE ART	RH0705						CONCUR A	8828
RESISTOR, CHIP	M55342K06R6K80S	MIL-R-55342/6	STATE OF THE ART	RH0705						CONCUR A	8820
RESISTOR, COMPOSITION	RCR05G100JS	MIL-R-39008/4	A-B	RCR05						N/R	8809
RESISTOR, COMPOSITION	RCR05G101JS	MIL-R-39008/4	A-B	RCR05						N/R	8816
RESISTOR, COMPOSITION	RCR05G102JS	MIL-R-39008/4	A-B	RCR05						N/R	8814
RESISTOR, COMPOSITION	RCR05G120JS	MIL-R-39008/4	A-B	RCR05						N/R	8815
RESISTOR, COMPOSITION	RCR05G131JS	MIL-R-39008/4	A-B	RCR05						N/R	8803
RESISTOR, COMPOSITION	RCR05G132JS	MIL-R-39008/4	A-B	RCR05						N/R	8818
RESISTOR, COMPOSITION	RCR05G150JS	MIL-R-39008/4	A-B	RCR05						N/R	8707
RESISTOR, COMPOSITION	RCR05G151JS	MIL-R-39008/4	A-B	RCR05						N/R	8829
RESISTOR, COMPOSITION	RCR05G152JS	MIL-R-39008/4	A-B	RCR05						N/R	8820
RESISTOR, COMPOSITION	RCR05G161JS	MIL-R-39008/4	A-B	RCR05						N/R	8810
RESISTOR, COMPOSITION	RCR05G180JS	MIL-R-39008/4	A-B	RCR05						N/R	8837
RESISTOR, COMPOSITION	RCR05G181JS	MIL-R-39008/4	A-B	RCR05						N/R	8818
RESISTOR, COMPOSITION	RCR05G182JS	MIL-R-39008/4	A-B	RCR05						N/R	8832
RESISTOR, COMPOSITION	RCR05G201JS	MIL-R-39008/4	A-B	RCR05						N/R	8840
RESISTOR, COMPOSITION	RCR05G202JS	MIL-R-39008/4	A-B	RCR05						N/R	8824
RESISTOR, COMPOSITION	RCR05G221JS	MIL-R-39008/4	A-B	RCR05						N/R	8828
RESISTOR, COMPOSITION	RCR05G240JS	MIL-R-39008/4	A-B	RCR05						N/R	8840
RESISTOR, COMPOSITION	RCR05G270JS	MIL-R-39008/4	A-B	RCR05						N/R	8829
RESISTOR, COMPOSITION	RCR05G271JS	MIL-R-39008/4	A-B	RCR05						N/R	8720
RESISTOR, COMPOSITION	RCR05G300JS	MIL-R-39008/4	A-B	RCR05						N/R	8813
RESISTOR, COMPOSITION	RCR05G301JS	MIL-R-39008/4	A-B	RCR05						N/R	8830
RESISTOR, COMPOSITION	RCR05G330JS	MIL-R-39008/4	A-B	RCR05						N/R	8813
RESISTOR, COMPOSITION	RCR05G331JS	MIL-R-39008/4	A-B	RCR05						N/R	8831

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EOS/AMSU SUBCONTRACTOR PRELIMINARY PARTS LIST

SPACEK

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART NUMBER	QTY	NSPAR	GSFC	DPA	DATE
					PER	NUMBER	NSPAR	STATUS	CODE
					SYS				
RESISTOR, COMPOSITION	RCR05G361JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8811
RESISTOR, COMPOSITION	RCR05G390JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8832
RESISTOR, COMPOSITION	RCR05G391JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8812
RESISTOR, COMPOSITION	RCR05G471JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8816
RESISTOR, COMPOSITION	RCR05G510JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8829
RESISTOR, COMPOSITION	RCR05G511JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8829
RESISTOR, COMPOSITION	RCR05G560JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8817
RESISTOR, COMPOSITION	RCR05G561JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8823
RESISTOR, COMPOSITION	RCR05G566JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8839
RESISTOR, COMPOSITION	RCR05G680JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8817
RESISTOR, COMPOSITION	RCR05G681JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8813
RESISTOR, COMPOSITION	RCR05G750JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8832
RESISTOR, COMPOSITION	RCR05G751JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8806
RESISTOR, COMPOSITION	RCR05G820JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8821
RESISTOR, COMPOSITION	RCR05G822JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8822
RESISTOR, COMPOSITION	RCR05G910JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8819
RESISTOR, COMPOSITION	RCR05G9R1JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	8841
TRANSISTOR, NPN	30020-1	30020	NEC	NE64508(B)	1	SP105-01B	CONCUR	A	8839
TRANSISTOR, NPN	30020-2	30020	NEC	NE02107E(B)(-1to-9)	1	SP105-02B	CONCUR	A	

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EOS/AMSU SUBCONTRACTOR PRELIMINARY PARTS LIST

AMPLICA

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART		QTY PER SYS	NSPAR NUMBER	GSFC NSPAR STATUS	DPA STATUS	DATE STATUS CODE
				NUMBER						
CAPACITOR, CHIP	76131-102	76131	AVX	CDR01BX102BKMS			STD	N/R	A	8919
CAPACITOR, CHIP	76131-472	76131	AVX	CDR01BX472AKMS			STD	N/R	A	8913
CAPACITOR, CHIP	76131-560	76131	AVX	CDR01BX560BJMS			STD	N/R	A	8925
CAPACITOR, CHIP	76132-0R5	76132	AVX	CDR128G0R5ABUR			STD	N/R	A	8914
CAPACITOR, CHIP	76132-130	76132	AVX	CDR128G130AFUR			STD	N/R	A	8840
CAPACITOR, CHIP	76132-150	76132	AVX	CDR128G150AFUR			STD	N/R	A	8848
CAPACITOR, CHIP	76132-160	76132	AVX	CDR128G160AFUR			STD	N/R	A	8908
CAPACITOR, CHIP	76132-1R5	76132	AVX	CDR128G1R5ABUR			STD	N/R	A	8817
CAPACITOR, CHIP	76132-1R8	76132	AVX	CDR128G1R8ABUR			STD	N/R	A	8749
CAPACITOR, CHIP	76132-200	76132	AVX	CDR128G200AFUR			STD	N/R	A	8830
CAPACITOR, CHIP	76132-2R4	76132	AVX	CDR128G2R4ABUR			STD	N/R	A	8751
CAPACITOR, CHIP	76132-300	76132	AVX	CDR128G300AFUR			STD	N/R	A	8914
CAPACITOR, CHIP	76132-4R3	76132	AVX	CDR128G4R3ABUR			STD	N/R	A	8901
CAPACITOR, CHIP	76132-4R7	76132	AVX	CDR128G4R7ABUR			STD	N/R	A	8749
CAPACITOR, CHIP	76132-5R1	76132	AVX	CDR128G5R1ABUR			STD	N/R	A	8903
CAPACITOR, CHIP	76132-5R6	76132	AVX	CDR128G5R6ABUR			STD	N/R	A	8748
CAPACITOR, CHIP	76132-6R2	76132	AVX	CDR128G6R2ABUR			STD	N/R	A	8813
CAPACITOR, CHIP	76132-7R5	76132	AVX	CDR128G7R5ABUR			STD	N/R	R	8806
CAPACITOR, CHIP	76132-7R5	76132	AVX	CDR128G7R5ABUR			STD	N/R	A	8906
CAPACITOR, CHIP	76132-8R2	76132	AVX	CDR128G8R2ABUR			STD	N/R	A	8803
CAPACITOR, CHIP	76132-9R1	76132	AVX	CDR128G9R1ABUR			STD	N/R	A	8907
CONNECTOR, SMA	600210	600210	OMNI-SPECTRA	2058-5029-00			AM131	CONCUR	A	8808
CONNECTOR, SMA	600210	600210	OMNI-SPECTRA	2058-5029-00			AM131	CONCUR	A	8817
DIODE	76141	76141	MOTOROLA	1N4625			AM111	CONCUR	A	8739
DIODE	JANS1N5415	MIL-S-19500/411 QPL		1N5415			STD	N/R	N/A	

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EOS/AMSU SUBCONTRACTOR PRELIMINARY PARTS LIST

AMPLICA

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART		QTY	NSPAR	GSFC	DPA	DATE
				MIL-SPEC PART	NUMBER					
				NUMBER		SYS	PER	STATUS		
FILTER	M15733/61-0008	MIL-F-15733/61	SPECTRUM CONTROLS	420066	AM127			CONCUR	A	8814
INDUCTOR	7981-20	7981	QPL		STD			N/R	N/A	
INDUCTOR	7981-40	7981	QPL		STD			N/R	N/A	
INDUCTOR	7981-50	7981	QPL		STD			N/R	N/A	
INDUCTOR	7981-55	7981	QPL		STD			N/R	N/A	
INDUCTOR	7985-20	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-25	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-30	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-35	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-40	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-50	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-80	7985	QPL		STD			N/R	N/A	
INDUCTOR	7985-90	7985	QPL		STD			N/R	N/A	
INDUCTOR	M39010/08810KS	MIL-I-39010/8			AM118-01			CONCUR	N/A	
INDUCTOR	M39010/08810KS	MIL-I-39010/8			AM118-02			CONCUR	N/A	
INDUCTOR	M39010/09A100KS	MIL-I-39010/9			AM117			CONCUR	N/A	
INDUCTOR	76137	76137	FAIRCHILD	M38510/119058PA	AM109A			CONCUR	A	8807
MCKT., OP-AMP	M55342M02R10J0M	MIL-R-55342/2			AM130-01			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R10K0R	MIL-R-55342/2			AM130-02			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R120JH	MIL-R-55342/2			AM130-03			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R150JH	MIL-R-55342/2			AM130-04			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R1K00M	MIL-R-55342/2			AM130-05			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R1K00R	MIL-R-55342/2			AM130-06			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R1K00R	MIL-R-55342/2			AM130-07			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R200JH	MIL-R-55342/2			AM130-08			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R2K00M	MIL-R-55342/2			AM130-09			CONCUR	N/A	
RESISTOR, CHIP	M55342M02R390JH	MIL-R-55342/2			AM130-10			CONCUR	N/A	

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EOS/ANSU SUBCONTRACTOR PRELIMINARY PARTS LIST

AMPLICA

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART NUMBER	QTY PER SYS	NSPAR NUMBER	GSFC NSPAR STATUS	DPA STATUS CODE	DATE
RESISTOR, CHIP	M55342M02R51J0R	MIL-R-55342/2		RH0505		AM130-11	CONCUR	N/A	
RESISTOR, CHIP	M55342M02R56J0H	MIL-R-55342/2		RH0505		AM130-12	CONCUR	N/A	
RESISTOR, CHIP	M55342M06R33J0H	MIL-R-55342/6		RH0705		SP086-06	CONCUR	N/A	
RESISTOR, COMPOSITION	RCR05G101JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G102JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G121JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G131JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G133JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G151JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G241JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G301JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G302JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G331JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G363JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G431JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G511JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G561JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G620JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
RESISTOR, COMPOSITION	RCR05G682JS	MIL-R-39008/4	A-B	RCR05		STD	N/R	N/A	
TRANSISTOR	320256	MIL-S-19500/291	QPL	2N2907A		STD	N/R	N/A	
TRANSISTOR	76140	76140	NEC	NE64508(8)		AM110A	CONCUR	A	8706
TRANSISTOR, FET	7541	7541	MITSUBISHI	MGF1412-29		AM106A	CONCUR	A/S	75AA
TRANSISTOR, FET	7543	7543	MITSUBISHI	MGF1801-33		AM107A	CONCUR	A	89AA

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EOS/ANSU SUBCONTRACTOR PRELIMINARY PARTS LIST

MAGTECH

PART DESCRIPTION	PART NUMBER	SPECIFICATION NUMBER	MANUFACTURER	VENDOR, GENERIC OR MIL-SPEC PART NUMBER	QTY PER SYS	NSPAR NUMBER	GSFC NSPAR STATUS	DPA STATUS	DATE STATUS CODE
MCKT.,HALL EFFECT SENSOR	25012/16-1	25012/16	SPRAGUE	UGS-3140HH	4	MT0278	CONCUR	R	90490
MCKT.,HALL EFFECT SENSOR	25012/16-1	25012/16	SPRAGUE	UGS-3140HH	4	MT0278	CONCUR	A/P	89268

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August 22, 1994

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/26-24

DESCRIPTION:

Provide impact assessment of updated NSPARs submittal criteria.

BACKGROUND

Since many of the parts will be the same, the preliminary parts list submitted for EOS was based largely on the latest PDIL for NOAA. It was also submitted with the negotiated understanding that all of the approved NOAA NSPARs would be acceptable on EOS. However, the effect of changes in part selection requirements is that some parts which required NSPARs on NOAA will not on EOS, and conversely, some that did not require NSPARs on NOAA will need them on EOS.

RESPONSE:

The EOS part selection requirement which will reduce the number of NSPARs is the definition that Grade 2 parts are "standard" if they are listed in either PPL 20 or MIL-STD-975. On NOAA, all Grade 2 parts required NSPARs. A review of the latest PDIL for NOAA was performed and 34 NSPARs/parts were identified which fall into the above category and, therefore, review/approval by NASA would not have been required.

The EOS part selection requirement which will increase the number of NSPARs is the definition that any part not listed on either PPL 20 or MIL-STD-975 is considered "non-standard". On NOAA, JANS level microcircuits/semiconductors and passive devices listed on a QPL were considered "standard" even if they were not listed on the PPL or MIL-STD-975. A review of the latest PDIL for NOAA indicated 31 parts which fall into the above category and, therefore, NSPARs would have been required.

Assuming the new parts selection requirements will result in similar plus/minus NSPAR numbers on EOS, the impact on labor was assessed. The elimination of 34 carry-over NSPARs would have no impact on planned effort by Aerojet Design Assurance since these documents

already exist and resubmittal would not be required. For NASA it means that those 34 NSPARs will not have to be reviewed/approved.

The need for 31 new NSPARs would require added labor to prepare and submit the NSPARs for NASA review/approval. Based on NOAA/AMSU-A experience each NSPAR requires approximately 5 manhours which calculates to a total of $5 \times 31 = 155$ manhours (SE-3).


Emil Lorenz Date 8/29/94

ACTION ITEM RESPONSE

FAXED 8/30/94

Action Item No: 7/27-1Action Requested:

What problem does going to 10V (from 8V) to the mixer/IF amp solve? Provide a list of SDARs. What is the supporting data that the problems are solved?

Response:

Out-of-specification conditions reported in the NOAA/AMSU-A mixer/IF amplifier units were attributed to the low operating voltage (+8.0V) and current budget as can be seen in the attached Supplier's Discrepancy Action Requests (SDARs). These SDARs are: 1) 1dB output compression point; 2) Gain versus voltage sensitivity; 3) Overall gain; 4) Gain versus temperature sensitivity; and 5) Gain flatness. The SDARs were approved based on a trade analysis as some other receiver components outperformed the specified requirements.

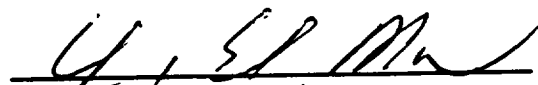
Although no supporting data for the specific performance improvements are available, the supplier (Spacek Labs, Inc.) expressed with confidence that the SDARs described above can be eliminated by increasing the bias voltage of the amplifiers from +8V to +10V. The following is the supplier's action plans to eliminate the SDARs imposed on the NOAA/AMSU-A to mixer/IF amplifiers.

- 1) 1dB output compression point:
With the additional voltage Spacek can ask Cougar Components who makes the output TO-8 cans to change the collector resistors to give a 1 dB output compression point of +10 dBm minimum.
- 2) Gain versus voltage sensitivity:
By raising the amplifier input voltage the gain versus voltage will definitely improve. In addition, the new specification is 2.5dB/Volt, which was the worst case on the previously delivered mixer/IF amplifiers, so there is no doubt that this SDAR will be eliminated.
- 3) Overall gain:
The 0.1dB out-of-specification condition (out of 59dB) of the -10 unit can readily be corrected with increased bias voltage as the gain of the transistors can be increased with bias voltage.
- 4) Gain versus temperature sensitivity:
Spacek anticipates improvement on the gain versus temperature sensitivity for the -10 unit as it can select more linear operating point of the unit with increased bias voltage.

5) Gain flatness:

With the additional voltage Spacek can select more linear operating point of the unit with frequency to improve the gain flatness.

Dash -1 through -8 units are for the channels 1 through 8, dash -9 unit for the channels 9 through 14, and dash -10 for the channel 15.


Y.E. Ma, Team Leader
Receiver Subsystem

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AEROJET ELECTROSYSTEMS COMPANY

10-009-030 Rev. 6-85

FOR SUPPLIER USE		FOR AESC USE	
1. SUPPLIER SDAR S/N	20	29. AESC SDAR S/N	
2. DATE SUBMITTED	5/10/90	30. DATE RECEIVED	

SUPPLIER'S DISCREPANCY ACTION REQUEST

TO BE COMPLETED BY SUPPLIER (Please Type or Print) THE SUPPLIER ACCEPTS FULL RESPONSIBILITY FOR ACCURACY OF INFORMATION BELOW:

3. SUPPLIER'S NAME AND ADDRESS SPACEK LABS, INC. 212 E. GUTIERREZ ST. SANTA BARBARA, CA 93101	4. SUPPLIER'S CODE 86472	5. BUYER'S CODE 43	6. CONTRACT NO. NAS5-29402	7. WORK ORDER NO. 2536-93-1000	8. P.O. NUMBER 06567
9. PART NUMBER 1331562-1A to 9A		10. PART NAME C/L Mixer-Amplifier Assembly	11. NEXT ASSY.		
12. Qty. on Order 50	13. Qty. of Ship 10	14. QTY. PAST DUE 40	15. PREVIOUS SDAR (DATE & NO.) 2-10-90		

16. Qty. 36	17. Ser'l Nos. { 9K01 - 9K09 9K11 - 9K19 9K21 - 9K29 9K31 - 9K39	18. CONDITION: The output 1.0 dB compression point on the dash -1A thru -9A amplifiers is measuring under 1.0 dB. The worst case reading is 8.2 dB	19. ACTION REQUESTED: Approve 1.0 dB output compression point of 8.0dB minimum for the flight units.	20. CAUSE & CORRECTION ACTION: (Include Effect, Date, Serial Numbers or Quantity of Parts Affected) This condition is caused by the low operating voltage +8.0 VDC and current budget, as well as an additional .1 volt drop across the S level protection diode. The condition can not be corrected without increasing the input voltage/Current, without trading off the amplifier gain and flatness. Rejection of this request would cause long schedule and delivery delays.
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(Attach Extra Sheets, Photographs, Sketches, etc., as Necessary)

21. SIGNATURE OF SUPPLIER'S AUTHORIZED REPRESENTATIVE: <i>William D. Neuman</i>	22. SDAR COPIES REQUIRED	23.	24. MODEL
TO BE COMPLETED BY AESC (Please Type or Print)			
25. COMMENTS OF SQR (or SPVR Receiving Inspection)/BUYER			

26. SIGNATURE OF SQR (or SPVR Receiving Inspection) DATE	27. SIGNATURE OF GOVT. REP. AT SOURCE (if Req'd) DATE	28. SIGNATURE OF BUYER	DATE
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31. DISPOSITION:

32. QUALITY CONTROL	DATE	33. ENGINEERING	DATE	34. CUSTOMER	DATE	35.
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SPECIAL INSTRUCTIONS TO SUPPLIER

1. FINAL APPROVAL OF THIS REQUEST SHALL APPLY ONLY TO THE ITEMS SPECIFIED HEREIN AND SHALL NOT ESTABLISH A PRECEDENT. ALL FINDINGS WILL BE SUBJECT TO VERIFICATION AND FINAL APPROVAL AT AESC.
2. WITHHOLD SHIPMENT PENDING RECEIPT OF APPROVED SDAR. FOR SHIP



AERJET ELECTROSYSTEMS COMPANY

10-400-430 Rev. 6-85

FOR SUPPLIER USE	FOR AESC USE
1. SUPPLIER SDAR S/N 21	29. AESC SDAR S/N
2. DATE SUBMITTED 5/10/90	30. DATE RECEIVED

SUPPLIER'S DISCREPANCY ACTION REQUEST

TO BE COMPLETED BY SUPPLIER (Please Type or Print) THE SUPPLIER ACCEPTS FULL RESPONSIBILITY FOR ACCURACY OF INFORMATION BELOW:

SUPPLIER'S NAME AND ADDRESS Spacek Labs, Inc. 212 E. Gutierrez St. Santa Barbara, CA 93101	4. SUPPLIER'S CODE 86472	5. BUYER'S CODE 43	6. CONTRACT NO. NAS5-29402	7. WORK ORDER NO. 2536-93-1000	8. P.O. NUMBER 06567
	9. PART NUMBER 1331562-1Ato10A	C/L	10. PART NAME Mixer-Amplifier Assembly		11. NEXT ASSY.
	12. Qty. on Order 50	13. Qty. of Ship 10	14. QTY. PAST DUE 40	15. PREVIOUS SDAR (DATE & NO.) 20 5/10/90	

16. Qty.	17. Ser'l Nos.	18. CONDITION:	19. ACTION REQUESTED:	20. CAUSE & CORRECTION ACTION: (Include Effectivity Date, Serial Numbers or Quantity of Parts Affected)
0	9K01 - 9K40	The gain versus voltage sensitivity of all amplifier dash numbers is measuring high, as were the engineering units. The worst case is 2.5 dB/volt.	Approve gain versus voltage sensitivity of 3.0 dB/volt maximum for the flight amplifiers.	<p>This condition is caused by the low operating voltage +8.0 VDC and current budget as well as an additional .1 volt drop across the S level protection diode.</p> <p>This condition can not be corrected without increasing the input voltage and current.</p> <p>Rejection of this request would cause long schedule and delivery delays.</p>

(Attach Extra Sheets, Photographs, Sketches, etc., as Necessary)

21. SIGNATURE OF SUPPLIER'S AUTHORIZED REPRESENTATIVE: <i>William J. Thompson</i>	22. SDAR COPIES REQUIRED	23.	24. MODEL:
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TO BE COMPLETED BY AESC (Please Type or Print)

25. COMMENTS OF SQR (or SPYR Receiving Inspection)/BUYER

26. SIGNATURE OF SQR (or SPYR Receiving Inspection) DATE	27. SIGNATURE OF GOVT. REP. AT SOURCE (If Req'd) DATE	28. SIGNATURE OF BUYER	DATE
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31. DISPOSITION:

32. QUALITY CONTROL	DATE	33. ENGINEERING	DATE	34. CUSTOMER	DATE	35.
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SPECIAL INSTRUCTIONS TO SUPPLIER

1. FINAL APPROVAL OF THIS REQUEST SHALL APPLY ONLY TO THE ITEMS TO VERIFICATION AND FINAL APPROVAL AT AESC.

2. WITHHOLD SHIPMENT PENDING RECEIPT OF APPROVED SDAR. FOR SHI

B-27

LEIN AND SHALL NOT ESTABLISH A PRECEDENT. ALL FINDINGS WILL BE SUBJECT

GATE MATERIAL SPECIFIED HEREON AND ATTACH COPY OF APPROVED SDAR.



AEROJET ELECTROSYSTEMS COMPANY

FOR SUPPLIER USE	FOR AESC USE
1. SUPPLIER SDAR S/N 22	29. AESC SDAR S/N
2. DATE SUBMITTED 5/10/90	30. DATE RECEIVED

SUPPLIER'S DISCREPANCY ACTION REQUEST

TO BE COMPLETED BY SUPPLIER (Please Type or Print) THE SUPPLIER ACCEPTS FULL RESPONSIBILITY FOR ACCURACY OF INFORMATION BELOW:

3. SUPPLIER'S NAME AND ADDRESS Spacek Labs, Inc. 212 E. Gutierrez St. Santa Barbara, CA 93101		4. SUPPLIER'S CODE 86472	5. BUYER'S CODE 43	6. CONTRACT NO. NAS5-29402	7. WORK ORDER NO. 2536-93-1000	8. P.O. NUMBER 06567
9. PART NUMBER 1331562-10A		C/L		10. PART NAME Mixer-Amplifier Assembly		11. NEXT ASSY.
12. Qty. on Order 50	13. Qty. of Shpt 10	14. QTY. PAST DUE 40	15. PREVIOUS SDAR (DATE & NO.) 21 5/10/90			
16. Qty.	17. Ser'l Nos.	18. CONDITION:		19. ACTION REQUESTED:	20. CAUSE & CORRECTION ACTION: (Include Effectivity Date, Serial Numbers or Quantity of Parts Affected)	
4	9K10 9K20 9K30 9K40	The -10 amplifier overall gain is reading as low as 58.9 dB. i.e. it is a 0.1 dB below the minimum overall gain spec. This condition occurs over the last 10 MHz of the I.F. pass band.		Approve -10 flight amplifiers with overall gains of 58.5 dB minimum.	This condition is caused by the low operating voltage +8.0 VDC and current budget, as well as by an additional .1 volt drop across the S level protection diode, and a typical drop of about .5 for each WJ can at 1550 MHz. To the greatest extent possible we have compensated for this in the tuning of the preamp. ifer stage. This condition can not be corrected without increasing the input voltage and current. Rejection of this request would cause long schedule and delivery delays	

(Attach Extra Sheets, Photographs, Sketches, etc., as Necessary)

21. SIGNATURE OF SUPPLIER'S AUTHORIZED REPRESENTATIVE: <i>William R. Neuman</i>	22. SDAR COPIES REQUIRED	23.	24. MODEL
TO BE COMPLETED BY AESC (Please Type or Print)			
25. COMMENTS OF SQR (or SPYR Receiving Inspection)/BUYER			

26. SIGNATURE OF SQR (or SPYR Receiving Inspection) DATE	27. SIGNATURE OF GOVT. REP. AT SOURCE (If Req'd) DATE	28. SIGNATURE OF BUYER	DATE
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31. DISPOSITION:

32. QUALITY CONTROL	DATE	33. ENGINEERING	DATE	34. CUSTOMER	DATE	35.
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SPECIAL INSTRUCTIONS TO SUPPLIER

1. FINAL APPROVAL OF THIS REQUEST SHALL APPLY ONLY TO THE ITEMS SPECIFIED TO VERIFICATION AND FINAL APPROVAL AT AESC.

IN AND SHALL NOT ESTABLISH A PRECEDENT. ALL FINDINGS WILL BE SUBJECT

2. WITHHOLD SHIPMENT PENDING RECEIPT OF APPROVED SDAR. FOR SHIPMENT

B-28

DATE MATERIAL SPECIFIED HEREON AND ATTACH COPY OF APPROVED SDAR.



AEROJET ELECTROSYSTEMS COMPANY

SUPPLIER'S DISCREPANCY ACTION REQUEST

FOR SUPPLIER USE	FOR AESC USE
1. SUPPLIER SDAR S/N 23	29. AESC SDAR S/N
2. DATE SUBMITTED 5/10/90	30. DATE RECEIVED

TO BE COMPLETED BY SUPPLIER (Please Type or Print) THE SUPPLIER ACCEPTS FULL RESPONSIBILITY FOR ACCURACY OF INFORMATION BELOW:

3. SUPPLIER'S NAME AND ADDRESS Spacek Labs, Inc. 212 E. Gutierrez St. Santa Barbara, CA 93101		4. SUPPLIER'S CODE 86472	5. BUYER'S CODE 43	6. CONTRACT NO. NAS5-29402	7. WORK ORDER NO. 2536-93-1000	8. P.O. NUMBER 06567
9. PART NUMBER 1331562-1Ato10A		C/L		10. PART NAME Mixer-Amplifier Assembly		11. NEXT ASSY.
12. Qty. on Order 50	13. Qty. of Shp't 10	14. QTY. PAST DUE 40	15. PREVIOUS SDAR (DATE & NO.) 22 5/10/90			

16. Qty. 40	17. Ser'l Nos. 9K01 - 9K40	18. CONDITION: The dash -1A thru -9A amplifiers appear to be reading right on spec. 0.02 db per degree C. The dash -10A amplifiers are reading 0.03 dB per degree C and are out of spec. by 0.01 dB per degree C. Since the graph data is subject to individual interpretation the dash -1A thru -9A should be given broader graph interpretation.	19. ACTION REQUESTED: Approve gain versus temperature maximum of 0.03 dB per degree C for the -1A to the dash -9A, and 0.05 dB per degree C for the -10A amplifiers.	20. CAUSE & CORRECTION ACTION: (Include Effectivity Date, Serial Numbers or Quantity of Parts Affected) This condition is caused by the low operating voltage +8.0 VDC and current budget, as well as by an additional .1 volt drop across the S level protection diode. This condition can not be corrected without increasing the input voltage and current. Rejection of this request would cause long schedule and delivery delays.
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(Attach Extra Sheets, Photographs, Sketches, etc., as Necessary)

21. SIGNATURE OF SUPPLIER'S AUTHORIZED REPRESENTATIVE: <i>William J. Newman</i>	22. SDAR COPIES REQUIRED	23.	24. MODEL:
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TO BE COMPLETED BY AESC (Please Type or Print)

25. COMMENTS OF SQR (or SPVR Receiving Inspection)/BUYER

26. SIGNATURE OF SQR (or SPVR Receiving Inspection) DATE	27. SIGNATURE OF GOVT. REP. AT SOURCE (If Req'd) DATE	28. SIGNATURE OF BUYER	DATE
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31. DISPOSITION:

32. QUALITY CONTROL	DATE	33. ENGINEERING	DATE	34. CUSTOMER	DATE	35.
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SPECIAL INSTRUCTIONS TO SUPPLIER

1. FINAL APPROVAL OF THIS REQUEST SHALL APPLY ONLY TO THE ITEMS SPECIFIED TO VERIFICATION AND FINAL APPROVAL AT AESC.

2. WITHHOLD SHIPMENT PENDING RECEIPT OF APPROVED SDAR. FOR SHIPMENT B-29

AND SHALL NOT ESTABLISH A PRECEDENT. ALL FINDINGS WILL BE SUBJECT

NOTE MATERIAL SPECIFIED HEREON AND ATTACH COPY OF APPROVED SDAR.

JUN 13 1990

P.2 707

16-009-436 Rev. C-15



AEROJET ELECTROSYSTEMS COMPANY

FOR SUPPLIER USE		FOR AESC USE	
1. SUPPLIER SBAR #/N	24	21. AESC SBAR #/N	90-096
2. DATE SUBMITTED	5/16/90	22. DATE RECEIVED	5/23/90

SUPPLIER'S DISCREPANCY ACTION REQUEST JUN 11 1990

TO BE COMPLETED BY SUPPLIER (Please Type or Print) THE SUPPLIER ACCEPTS FULL RESPONSIBILITY FOR ACCURACY OF INFORMATION BELOW

3. SUPPLIER'S NAME AND ADDRESS		4. SUPPLIER'S CODE	5. BUYER'S CODE	6. CONTRACT NO.	7. WORK ORDER NO.	8. P.O. NUMBER
Spacek Labs, Inc. 212 E. Gutierrez St. Santa Barbara, CA 93101		86472	43	NAS5-29402	2536-93-1000	06567
9. PART NUMBER		10. QTY. ON ORDER	11. QTY. OF SHIP	12. QTY. PART DUE	13. PREVIOUS SBAR (DATE & NO.)	
1331562-1Ato-10A		50	10	40	23 5/10/90	
14. PART NAME				15. NEXT ASBY.		
Mixer-Amplifier Assembly						

16. QTY.	17. Ser'l No.	18. CONDITION	19. ACTION REQUESTED	20. CAUSE & CORRECTION ACTION (Include Effect, Date, Serial Number or Quantity of Parts Affected)
32	9K01 9K04 ... 9K10 9K11 9K14 ... 9K20 9K21 9K24 ... 9K30 9K31 9K34 ... 9K40	The dash -1A, and dash -4A thru -9A amplifiers are reading just in spec or over spec for gain flatness by .2dB worst case. The dash -10A amplifier is measuring out of spec for gain flatness by .6dB worst case. See attached amplifier summary sheet for measurements.	Accept a gain flatness for the dash -1A thru -9A amplifiers of .9dB peak-to-peak, and 2.0dB peak-to-peak for the dash -10A amplifier.	This condition is caused by the low operating voltage of +8.0 VDC and current budget, as well as by an additional .1 volt drop across the protection diode. Additionally for the -10A the 3 TO-8 amplifier cans have up to .5dB drop per can at 1550 MHz. This condition can not be corrected without increasing the input voltage/current. Rejection of this request would cause long schedule and delivery delays.

(Attach Extra Sheets, Photographs, Sketches, etc., as Necessary)

21. SIGNATURE OF SUPPLIER'S AUTHORIZED REPRESENTATIVE	22. SBAR COPIES REQUIRED	23.	24. MODEL
<i>William R. Neiman</i>			

TO BE COMPLETED BY AESC (Please Type or Print)

25. COMMENTS OF SQR (or SPYR Receiving Inspection)/BUYER

26. SIGNATURE OF SQR (or SPYR Receiving Inspection) DATE	27. SIGNATURE OF GOVT. REP. AT SOURCE (If Req'd) DATE	28. SIGNATURE OF BUYER DATE
		<i>[Signature]</i> 5/24/90

29. DISPOSITION:

30. QUALITY CONTROL	DATE	31. ENGINEERING	DATE	32. CUSTOMER	DATE	33.
						31/32

1. FINAL APPROVAL OF THIS REQUEST SHALL APPLY ONLY TO THE ITEM TO VERIFICATION AND FINAL APPROVAL AT AESC.

2. WITHHOLD SHIPMENT PENDING RECEIPT OF APPROVED SBAR. FOR B-30 SEGREGATE MATERIAL SPECIFIED HEREON AND ATTACH COPY OF APPROVED SBAR

RTK. NO. A-5-01

AMPLIFIER ELECTRICAL TESTS

UNIT	OVERALL GAIN		GAIN FLATNESS		GAIN VS. VOLT		GAIN VS. TEMP		1dB COMPRESSION	
	SPEC	MEAS	SPEC	MEAS	SPEC	MEAS	SPEC	MEAS	SPEC	MEAS
K01	70 ±1	IN SPEC	0.6dB ppk	0.6	0.5dB/V	<u>2.5</u>	0.02 dB/°C	0.02	+10dBm	9.0
K02	72 ±1	IN SPEC		0.2		2.0		0.02		9.4
K03	72 ±1	IN SPEC		0.5		2.0		0.02		9.4
K04	70 ±1	IN SPEC		<u>0.8</u>		2.0		0.02		9.8
K05		IN SPEC		0.5		2.5		0.02		9.5
K06		IN SPEC		0.6		2.0		0.02		9.5
K07		IN SPEC		0.6		2.0		0.02		9.3
K08		IN SPEC		0.4		2.0		0.02		9.7
K09	60 ±1	IN SPEC		0.6		2.0		0.02		8.9
K10	60 ±1	<u>58.9</u>	1.2dB ppk	1.7		1.0		<u>0.03</u>		11.5
K11	70 ±1	IN SPEC	0.6dB ppk	0.7		2.0		0.02		8.3
K12	72 ±1	IN SPEC		0.4		2.0		0.02		9.0
K13	72 ±1	IN SPEC		0.3		2.0		0.02		9.3
K14	70 ±1	IN SPEC		0.7		2.0		0.02		9.3
K15		IN SPEC		0.7		2.0		0.02		9.1
K16		IN SPEC		0.7		2.0		0.02		8.8
K17		IN SPEC		0.6		2.0		0.02		9.5
K18		IN SPEC		0.6		2.0		0.02		9.3
K19	60 ±1	IN SPEC		0.6		2.0		0.02		<u>8.2</u>
K20	60 ±1	IN SPEC	1.2dB ppk	<u>1.0</u>		1.5		0.03		11.5

NOTE: ALL UNITS MEET OUT OF BAND GAIN SPEC OF 740dBc.

OUT OF SPEC

WORST CASE

ACTION ITEM RESPONSE

8/11/94
TO M.D.M.E.S.
DURING VISIT.

ACTION ITEM NO. 7/27-3

ACTION REQUESTED:

Be sure that bolts used on TIROS spacecraft are specified in the ICD.

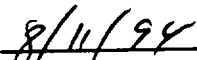
RESPONSE:

The NOAA/AMSU ICD has been reviewed. The following paragraph has been incorporated into the ICD (Draft) to describe the bolts used on the TIROS spacecraft.

3.4.3 Mounting Hardware

The mounting hardware is described in English units (inches) because EOS AMSU-A has heritage to the NOAA AMSU-A instruments. The Spacecraft Contractor shall provide all instrument mounting hardware. The mounting hardware is defined as a) No. 10 (.190 inches dia) Socket Head Cap Screws capable of withstanding 85 in-lbs of installation torque, b) No. 10 metal washers and c) fiberglass thermal washers. The final assembly of the mounting hardware as it relates to the AMSU-A instruments is as shown in Figure 3.4.3-1. The required dimensions of the fiberglass thermal washers are shown on Figure 3.4.3-2.

for 
Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader


Date 8/11/94

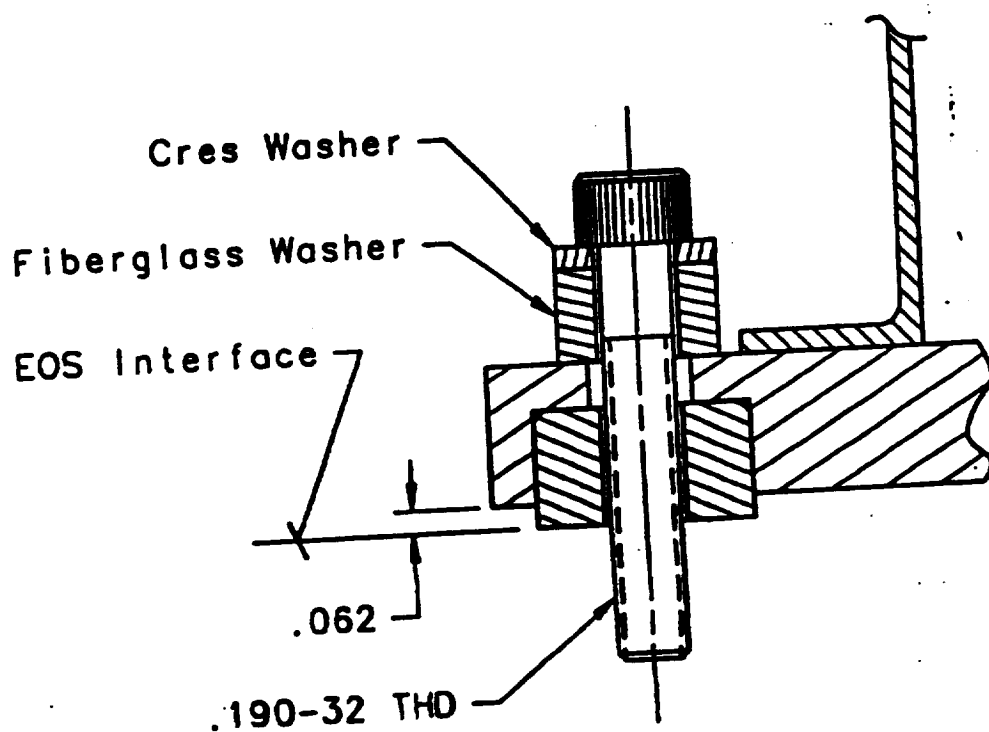


Figure 3.4.3-1 AMSU-A Mounting Hardware

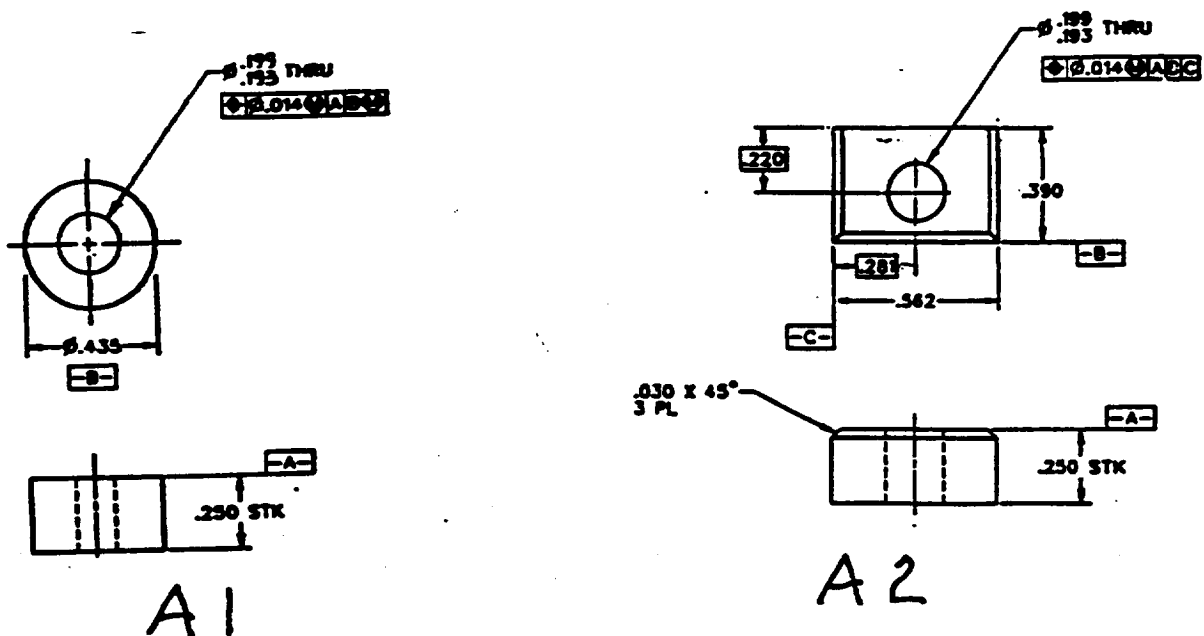


Figure 3.4.3-2 Thermal Washer Dimensions

ACTION ITEM RESPONSE

ACTION ITEM NO: 7/27-4

ACTION REQUESTED: Should the edge stiffening be implemented on the A2 to raise the natural frequency from 80 Hz on the NOAA unit to 90 Hz on the EOS unit? What is the trade between having to do additional analysis because we are less than 100 Hz and trying to get to 100 Hz? Include cost to do design change (including all paper and tests) and what is saved in production. Look at weight margin of N & N'.

RESPONSE: In preparation for the EOS AMSU-A PDR, the A2 structural math model was changed to include edge stiffening and natural frequency analyses were conducted. Removing the mass of the momentum compensator had a small (~1 Hz) effect on natural frequency. The combined effect of edge stiffening and compensator mass removal was to raise the natural frequency to 90.5 Hz. The weight penalty for the edge stiffener has been previously reported to be 2 pounds. Aerojet believes that the measured frequency will be slightly higher because the modeling of the base/side panel joint flexibility has remained conservative.

Aerojet had anticipated that the natural frequency could be raised above 100 Hz. Approximately 2 weeks of additional dynamic analysis were undertaken to find ways to raise the natural frequency. These efforts were unsuccessful because of the self-imposed constraints of "no major changes." Further natural frequency increases could be undoubtedly be obtained by increasing the thickness and stiffness of the honeycomb baseplate or increasing the number of spacecraft attachment bolts.

The scope of work remaining to change the EOS AMSU-A2 baseplate edge stiffener is 1)draw and release a replacement for PN1331211, Baseplate Assembly, Honeycomb and 2)incorporate the new part at the next assembly, PN 1331303, Antenna Subassembly, Machined A2. The estimated hours are:

<u>Skill</u>	<u>Hours</u>
Draftsman	40
Checker	20
Engineering Sign-off	<u>15</u>
	75

Since the EOS A2 NASTRAN model currently has edge beams, proceeding with solid edge beams will save effort to remove the solid beams from the model. Changing the beams is simple, but the new model would still have to be subjected to the 3 pages of GIRD check cases.

<u>Activity</u>	<u>Hours</u>
NASTRAN model Checks	(60)

The solid edge stiffener would save Honeycomb Baseplate fabrication time. Currently, the edge stiffener has a channel cross-section between the mounting bolt pads. The NOAA edge stiffener starts as a solid that is milled into a channel between the mounting bolt pads. The estimated savings are shown below:

<u>Activity</u>	<u>Hours</u>
N/C Programming (Non-recurring)	20)
N/C Milling (Recurring)	(25)
Inspection (Recurring)	(5)
	(50)

The cost analysis shows that the break even point for continuing with the solid edge beam is less than one unit.

The work required to increase the EOS AMSU-A2 above 100 Hz would require additional dynamic analyses to define the required changes. The assumption for the cost estimates are that the baseplate would be thickened and stiffened, and that the mounting hole pattern would change. This would require new baseplate, interface drill jig, interface control, and machined subassembly drawings. The handling procedure would also require changing.

<u>Skill</u>	<u>Hours</u>
Dynamicist	120
Draftsman	160
Checker	80
Specification Writer	40
Design Engineers	<u>80</u>
	480

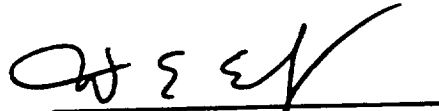
The response to Action Item 5/11-2 detailed the effort required to test and document the NOAA AMSU-A2 natural frequency of approximately 81 Hz. The man-hours for repeating the activity for EOS should be approximately 3/4 of the time expended on NOAA because the first modeshape is now well understood and test set-ups providing little pertinent data can be eliminated. Eliminating the need for testing will save:

<u>Skill</u>	<u>Hours</u>
Dynamicist	(120)
Test Engineer	(90)
Test Technician	(90)
NASTRAN Analyst	<u>(180)</u>
	(480)

If nothing is done to change the NOAA baseplate, this testing effort would be repeated for the EOS AMSU-A2. The removal of the momentum compensator is enough to change the natural frequency from that previously measured.

The maximum specified weight for the A2 unit is 104.5 pounds. The actual NOAA A2 weight is 103.0 pounds. The added weight for the edge stiffener of 2.0 pounds would lift the unit weight above the maximum allowed weight.

The probability of achieving 100 Hz on the NOAA A2 modules cannot be answered without first defining new constraints (e.g. weight) and then performing additional analysis. The estimated effort would be greater than that stated above (480 Hours) because of the design constraints.



Wayne Ely, Team Leader
EOS Mechanical/Thermal

8/29/94

EOS/AMSU-A Action Item Response

Action Item No. 7/27-6:

Description:

Determine basis for 1553 RT validation plan.


Response:

The validation plan for the MIL-STD-1553 interface is based on the need to validate the following six key functions:

- Process instrument commands.
- Process timing data from the spacecraft and derive 8 second frame pulses.
- Format science data into MIL-STD-1553 data packets and install at RAM subaddresses 1 through 16.
- Format engineering data into MIL-STD-1553 data packets and install at RAM subaddresses 17 through 20.
- Create data checksum.
- Append special header to start of data block.

The verification process is an end to end checkout of the entire interface CCA. It demonstrates the ability of the EOS/AMSU-A signal processor to handle commands and data via the MIL-STD-1553 interface. Specific MIL-STD-1553 transceiver functions are validated only to the extent that they contribute to this end to end test. This philosophy is based on the fact that a commercially available multi-chip module has been selected to perform all the transceiver and bus specific functions. This device will be purchased under an Aerojet Specification Control Drawing that will ensure it is validated by the manufacturer to meet all performance requirements. The interface designed by Aerojet is essentially a means of coupling this device to the EOS/AMSU-A signal processor.

Final verification of the MIL-STD-1553 interface will come when it is tested using the GFE Spacecraft Simulator. In this test it is planned to exercise all interface functions and apply all possible I/O conditions.


M.M.Pluck

Aug 2 1994
Date

EOS/AMSU-A Action Item Response

Action Item No. 7/27-7:

Description:

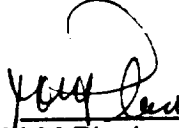
Define current threshold on A/D converter dropout.

Response:

The A/D Converter dropout referred to in the description above is a circuit designed to interrupt power to the A/D converter microchip in the event a latchup condition occurs due to heavy particle bombardment. This latchup condition is analogous to the 'ON' state of an SCR and normal operation can only be retrieved by the removal of power. Failure to react rapidly to a latchup condition can result in permanent thermal damage to the microchip.

The latchup circumvention circuit used in the AMSU-A signal processor is designed to trigger when the supply current to the A/D converter microchip exceeds 130mA. Normal operational current is 12mA and maximum current under worst case conditions is 25mA. Sustained current in a latchup condition is 275mA. The triggering threshold is therefore at a current more than 5 times greater than the maximum current likely to be experienced in normal operation.

In order to avoid false triggering due to the inrush current when power is first applied, a 4mS delay circuit is incorporated. Typical settling time for the inrush current is 1mS.


M.M.Pluck Aug. 9 1994
Date

ACTION ITEM RESPONSE

From the Desk of:

D. W. Howell
x1039

August 9, 1994

ACTION ITEM NO. 7/27-8

*FAVED
8/5/94*

To: Gus Wessels/NASA

Gus,

As a follow-up to our discussion regarding MRP training (and in response to Action Item 7/27-8), we can have a training session anytime it's convenient for you. All classes are custom scheduled. Just give me a couple of weeks notice and I'll set it up.

We can do either a one-day, six-hour version or two days with three hours each day. It will include both lecture and demonstration. (There is another version that includes hands-on training - 12 hours long, for direct users - but I don't think we need that.)

I'll probably join you since I also need to get "up-to-speed". Let me know what will work out for you.

Thanks.



D. W. Howell
Program Manager
EOS/AMSU-A Program

CC: M. Domen/NASA
A. Nieto/Aerojet
B. Terrell/Aerojet
R. Singer/Aerojet

GENCORP
AEROJET

8 August 1994


EOS/AMSU-A Action Item Response**Action Item 7/27-9****Description:**

Define what it takes to upgrade the CSTOL workstation to be capable of doing the complete instrument functions at the spacecraft contractors (not just listen only).


Response:

By adding an available 1553B SBus Serial interface module (EDT part # S53B-1) to the selected Sun SPARC machine, the Spacecraft Interface Workstation (SIW) could communicate with and receive data from the AMSU units via the 1553B interface. The SIW would act as the Bus Controller during unit test. If the units were being controlled by the spacecraft Bus Controller, the SIW would revert to a Remote Terminal configuration and perform as a receive-only station, receiving and processing AMSU data outputs. Since the power supply and power distribution of the Special Test Equipment (STE) for the AMSU units is freestanding and manually controlled, power to the AMSU units could be provided either by the Spacecraft or an included power supply subsystem in the SIW. Figure 1 is a simplified interconnect diagram of the SIW and Figure 2 is a sketch of a possible packaging of the SIW.

The added power supply, power distribution module, unit interface and cabling would be identical in design to that used in the STE, therefore, additional design efforts would be expended only on packaging and CSTOL software expansion to include unit control functions. Additional material costs would include purchasing of the 1553B bus interface card, the power supply, the PRT logger, the desk rack and parts for fabrication of the Power Distribution module, unit interface and interconnecting cables.


D. W. Howell Date 8/9/94


D. S. McDonald Date 8/8/94


R. W. Schwantje Date 8/8/94

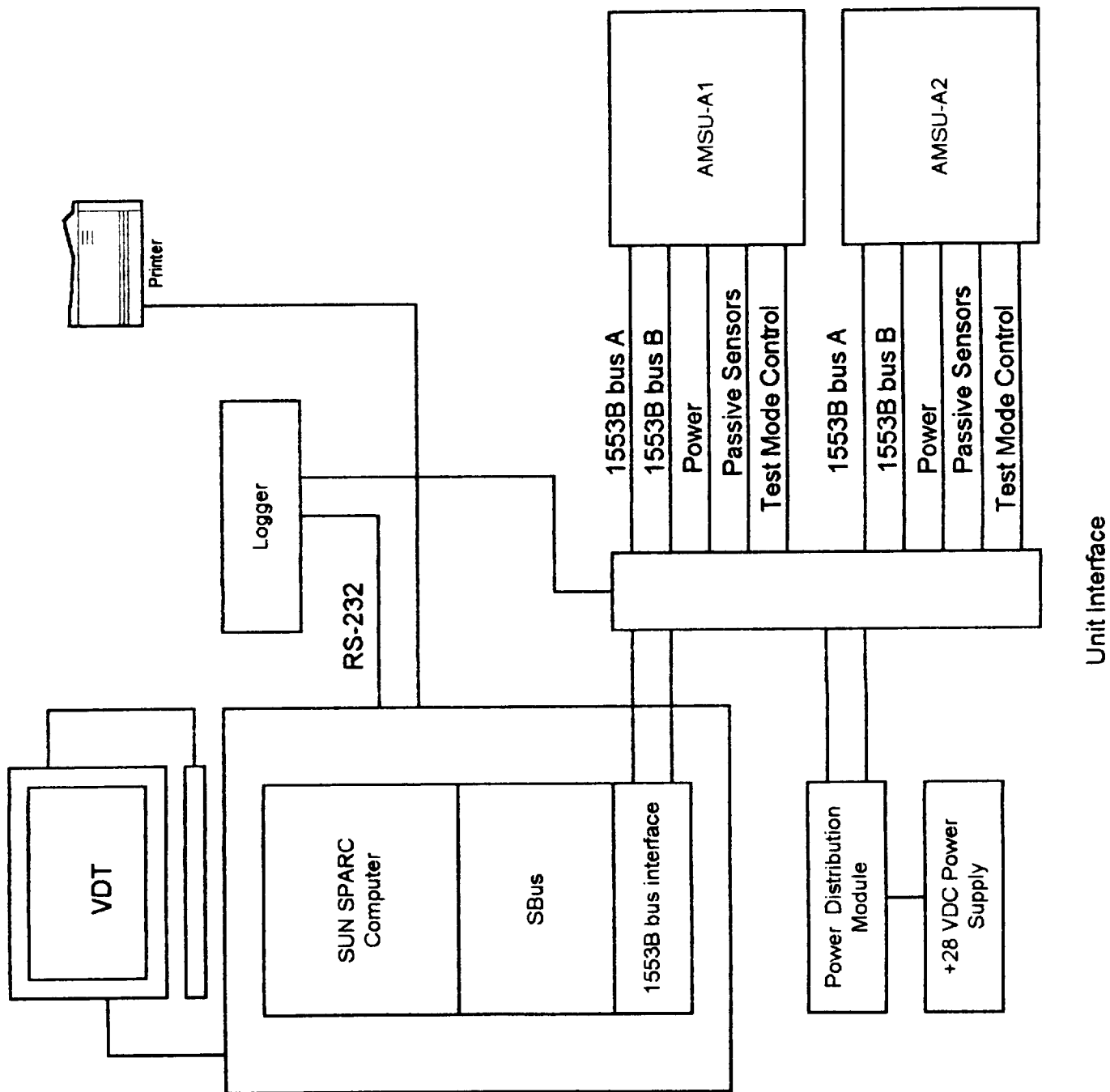


Figure 1 Spacecraft Interface Workstation

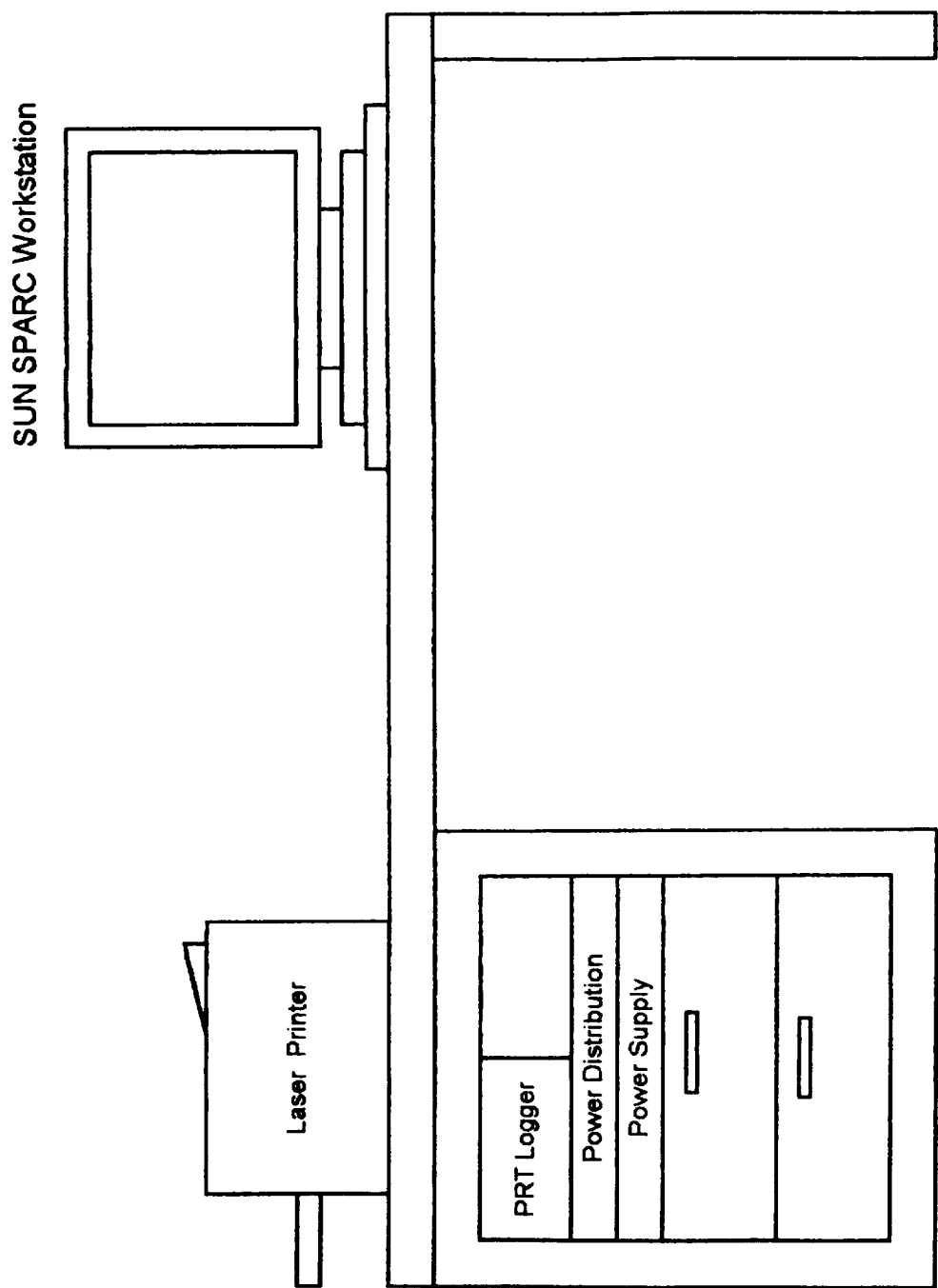


Figure 2 Physical Layout of Spacecraft Interface Workstation

ACTION ITEM RESPONSE

ACTION ITEM NO: 7/27-10ACTION REQUESTED:

Review pyroshock and sine burst requirements and applicability to component and instrument.

RESPONSE:1. Sine Burst

The sine burst test can be traced to the structural verification section (3.4.3.1) in the PAR. The structural verification method is not specified in the PAR. The requirement is that the structural verification shall be accomplished by a combination of analysis and test. The usual method is to apply a set of loads to the structure.

EOS AMSU-A will use the same method of structural verification as was used on NOAA AMSU-A --the sine burst test. The test is conducted at a frequency that is approximately 1/3 the first natural frequency of the instrument. Consequently, there is no amplification or attenuation through the structure and the components see the same levels as are introduced at the instrument mounting interface.

The GIRD requirements regarding structural verification of components are for either analysis or test. If components were qualified in a sine burst test, the level would be 21 g's peak. However, the AMSU-A components are also required to pass a random vibration test at 19.96 Grms. Statistically, the component may see peaks that are 3 times the Grms value. In addition, the random vibration extends from 20 to 2000 Hz and most likely excites the first several natural frequencies of the component.

Considering the above comparison, the random vibration test is a much more severe test than the sine burst test at the component level. Consequently, the sine burst can be eliminated with no risk to the components.

Aerojet is therefore proceeding to delete all sine burst test requirements from the component specifications, with the exception of the A2 Antenna.

2. Pyroshock Testing

The pyroshock environment is defined in paragraph 10.4 of the GIRD. The PAR (Table 3-1) requires a test at the instrument level but not at the component level.

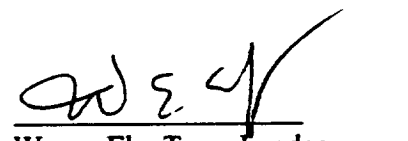
The pyroshock environment currently included in the AMSU-A component specifications is identical with that specified at the instrument mounting surface. This is a conservative flowdown of the shock requirements. Since the AMSU-A instruments have fundamental structural frequencies of approximately 100 Hz, the peak shock level of 1200 g's starting at 1150 Hz is significantly attenuated. In other words, the structure acts as a band-pass filter that minimizes transmission of high frequency energy.

The ideal solution would be to place accelerometers on the instrument and measure the transmission of shock to the components when the environment is applied at the module mounting interface. The measured shocks would then be inserted in the component specs, thus eliminating the risk of overtesting the components because of unknown structural attenuation. Unfortunately, this solution cannot be accomplished because 1) there are no EOS Engineering Models and 2) the instrument tests would occur long after the components would have been procured.

An alternate approach is to follow the PAR and not perform shock tests on the components. The risk is that shock-sensitive components may fail when the instruments are shock tested. However, the current shock curve appears to be representative of an environment that is relatively close to the pyro devices. High frequency shocks are attenuated rapidly as a function of the distance from the pyro device. Also, most components are mounted on thermal isolators which further mitigate the shock levels.

It is therefore felt that the risk of overtesting components in the currently-specified environment is higher than the risk of damaging components at the instrument level shock test. Accordingly, Aerojet will proceed to eliminate the pyroshock test requirements from the component specifications.


Weldon Chapman
Technical Director


Wayne Ely, Team Leader
Mechanical/Thermal Subsystem

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/27-11

ACTION REQUESTED:

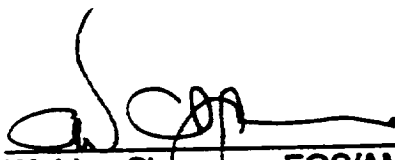
Flowdown to suppliers' requirement for N2 atmosphere during thermal cycling tests.

RESPONSE:

This action is being accomplished by modifying the thermal cycling test description, paragraph 4.6.3.2, of the environmental specification, AE-26578. This specification is referenced as part of each component procurement.

The following sentence will be added between the first and second sentences of paragraph 4.6.3.2 prior to awarding procurement contracts.

The atmosphere within the chamber shall be dry nitrogen or other inert dry gas to protect the unit under test from condensation related damage.


Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader

8/31/94
Date

ACTION ITEM RESPONSE

ACTION ITEM NO. 7/27-12

ACTION REQUESTED:

Develop and maintain a list of differences between N/N' and EOS, e. g., components, major active devices, etc.

RESPONSE:

A table indicating the differences is attached. The table will be modified and provided to the EOS Technical Officer as additional changes evolve.



Weldon Chapman, EOS/AMSU-A
Systems Engineering Product
Team Leader

8-4-94
Date

DIFFERENCES BETWEEN AMSU-A FOR EOS AND FOR N & N'

CHANGE TO EOS/AMSU-A	REASON FOR CHANGE/COMMENTS
MECHANICAL STRUCTURE AND THERMAL DESIGN	
Relocate A1 Mounting surface from side to base.	Requirement Change: EOS requires base mount.
Eliminate compensator in A2.	Disturbance torque requirement can be met without the compensator - In NOAA/AMSU It cannot.
Relocate optical alignment cubes near to base of A1 and A2.	Requirement in EOS GIRD that cubes be near base.
Thermal blanketing, mirror coverage on both A1 and A2 will (probably) differ	Modified to accommodate different orbit and spacecraft environment
DIGITAL PROCESSOR (A1 & A2)	
Replace Spacecraft Interface No. 1, Spacecraft Interface No. 2, and Parallel-to-Serial Converter CCAs with MIL-STD-1553B Bus Interface CCA.	Requirement Change: EOS requires MIL-STD-1553 Interface Instead of unique NOAA/AMSU Interface.
-change instrument firmware.	Different spacecraft Interface forces revision of a small percentage of code.
ANALOG PROCESSOR (A1 & A2)	
Design new engineering data multiplexer CCA to replace analog housekeeping and power relay CCAs	Requirements change: Engineering data must be on MIL-STD-1553 bus. Power relay CCA eliminated by combining functions on new CCA.
Change operating range of warmload temperature sensor conditioning circuits for A2 from 0°C - 20°C to 10°C - 30°C	Thermal analysis shows A2 to have different operational warmload temperature range in the EOS orbit.
SIGNAL PROCESSING (A1 & A2)	
Revise Signal Processing Assembly backplane wiring.	Driven by changes in spacecraft Interface to a MIL-STD-1553 bus.
Eliminate upper card rack in A1.	Cost improvement permitted by reduction in CCA count due to new Interface design.
POWER SUBSYSTEM (A1 & A2)	
Replace power relay assembly with new control/distribution module.	Requirements change: Power on/off not controlled by instrument as in NOAA/AMSU-A and redundant power bus is specified.

DIFFERENCES BETWEEN AMSU-A FOR EOS AND FOR N & N' (cont)

INTERCONNECTING HARNESS SUBSYSTEM (A1 & A2)	
Redesign main instrument harness so that it is in separate functional harnesses instead of one.	Harness redesign is necessary as a result of changing to the MIL-STD-1553 interface, changing the power interface, and adding the engineering data mux. Redesign using separate harnesses to provide cost savings due to simpler and much faster harness/unit integration.
Add connectors to receiver shelves.	Compatibility with new harness design plus cost savings due to faster system integration.
Eliminate power distribution panels.	Not necessary due to harness redesign.
Change A1 card rack card guides so that slot J303 accepts a CCA instead of an I/O card.	I/O card count reduced from five to four in existing NOAA/AMSU-A. Empty I/O slot is now needed for active CCA.
Replace analog telemetry temperature sensors (type AD 590) with redundant platinum resistance transducers.	Requirements change to match spacecraft passive analog signal inputs.
Install two thermal switches in series for each survival heater.	Safety: Survival heater power is 'on' all the time on EOS/AMSU whereas in NOAA/AMSU-A it is switched. If a heater thermal switch sticks 'on', the other switch will still be able to shut off the power, avoiding the possibility of overheating.
Eliminate compensator motor driver CCA.	Compensator requirement eliminated.
Change number and assignment of instrument to spacecraft connectors.	Requirement driven; in new C&DH and power interfaces.

APPENDIX C

SYSTEM ENGINEERING **INTERNAL DESIGN REVIEW**

SYSTEMS ENGINEERING INTERNAL DESIGN REVIEW

24 August 1994

A program of internal design reviews was begun this month, initiated with a system-level review. The review was well-attended, and included attendees from outside the program.

The following personnel attended. The functions/titles of those reviewers not directly attached to EOS/AMSU-A are provided.

Scott Armstrong, Aerojet Director of Sensor Products Engineering
Dennis Brest
Glen Crosby
Kala Crosby
Wayne Ely
Bob Hauerwaas, Technical Director of NOAA/AMSU-A
Sev Herrera
Glenn Martner
Al Nieto
Terry O'Brien, Aerojet Director of Systems Engineering
Prabodh Patel, NOAA/AMSU-A Systems Engineering Product Team Leader
Mark Pluck
Armando Valdez
Bob Newhouse, Aerojet Electronic Systems Manager

The presentation consisted of the following topics:

- a. EOS/AMSU-A Science Objectives and Mission Concept
- b. A System Overview - NOAA/AMSU-A vs EOS/AMSU-A
- c. Requirements Verification Flowdown Approach
- d. EOS/AMSU-A Systems Requirements as Imposed by GSFC
- e. Radiometer Performance and Budget Allocations
- f. EOS/AMSU-A System Concept
- g. EOS/AMSU-A Requirements Flowdown
- h. Environmental Requirements

Numerous points were raised which led to discussions and clarifications. Several other points were raised which resulted in issues which are still to be resolved. The following action items resulted:

1. A requirement imposed on NOAA/AMSU-A that beamwidth variations from channel to channel not vary by more than 10 percent total is not imposed on EOS/AMSU-A. A ± 10 percent requirement instead is imposed. This is a change that was imposed on NOAA/AMSU-A via a NASA program directive that did not make its way into the EOS/AMSU-A specification. Scientifically, should it also be imposed on EOS/AMSU-A?
2. The elimination of the upper card rack in the A1 module has been challenged because of its structural and, to a larger extent, its thermal conductivity value. The cage may thus be retained but not used, incurring a

slight weight increase. Is there a reasonable alternative to retaining the card cage, or should it be retained as is?

3. The use of a 143-MHz crystal oscillator as a primary source for the phase-locked oscillator in A1 which is outside the PLO package has lead to concerns about EMI, specifically because the 143-MHz frequency is within most channel IF passbands. The existing oscillator is double shielded and up-converted to a frequency outside the IF passbands to avoid EMI. Although the new design has carefully considered EMI in its design, NOAA/AMSU-A systems engineering has voiced concern. Examine the EMI concerns, and the feasibility and value of repackaging the PLO oscillator into a common package.
4. The EOS/AMSU-A instrument requires thermal-vacuum testing at -30°C to meet PAR requirements. Concern has been voiced as to our ability to cool an instrument to that level in vacuum in current facilities. Investigate the concern, establish its validity and if necessary establish an alternate approach to meeting the requirement.
5. RF components are specified to operate between 10°C and 30°C (with a 10°margin on both sides). RF shelves are predicted to be between 10°C and 30° in orbit, whereas there are electrical isolators between the shelves and components which would make the components operate at a higher temperature. Should the component specifications be modified to match the different range?

Responsibilities and a schedule for action item completion are being established, and the action items will be reported at PDR.

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6. AUTHOR(S) Donald Howell				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Aerojet 1100 W. Hollyvale Azusa, CA 91702			8. PERFORMING ORGANIZATION REPORT NUMBER CDRL 529 10300-12 September 1994	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) NASA Goddard Space Flight Center Greenbelt, Maryland 20771			10. SPONSORING/MONITORING AGENCY REPORT NUMBER - - -	
11. SUPPLEMENTARY NOTES - - -				
12a. DISTRIBUTION/AVAILABILITY STATEMENT - - -			12b. DISTRIBUTION CODE - - -	
13. ABSTRACT (Maximum 200 words) This is the twentieth monthly report for the Earth Observing System/Advanced Microwave Sounding Unit-A (EOS/AMSU-A), Contract NAS5-32314, and covers the period from 1 August 1994 through 31 August 1994. This period is the eighth month of the Implementation Phase which provides for the design, fabrication, assembly, and test of the first EOS/AMSU-A, the Protoflight Model. During this period, the primary activity was the procurement for long-lead items.				
14. SUBJECT TERMS EOS Microwave System			15. NUMBER OF PAGES 103	
			16. PRICE CODE - - -	
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7. Author(s) Donald Howell		8. Performing Organization Report No. 10300-12 September 1994	
		10. Work Unit No. ---	
9. Performing Organization Name and Address Aerojet 1100 W. Hollyvale Azusa, CA 91702		11. Contract or Grant No. NAS 5-32314	
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